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OGDEN AIR LOGISTICS CENTER

UNITED STATES AIR FORCE

HILL AIR FORCE BASE, UTAH 84406

2 147

PROPELLANT
SURVEILLANCE REPORT
LGM-30 A&B STAGE 1
TP-H1011

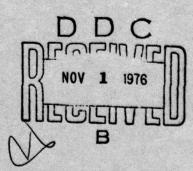
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PROPELLANT LAB SECTION

MANCP REPORT

NR 351 (76)

SEP 1976



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MANCP REPORT NR 351(76)
MMEMP PROJECT M72632-5MP116P

PROPELLANT SURVEILLANCE REPORT

LGM-30 A & B STAGE I

TP-H1011

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United States Air Force
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ABSTRACT

This report contains propellant test results from cartons of TP-H1011 bulk propellant representing LGM-30 A and B First Stage Minuteman Motors. This report is the eleventh time that a statistical approach has been used to analyze First Stage bulk carton propellant. Testing was accomplished in accordance with MMEMP Project M72632 - 5MP116P.

The purpose of testing was to determine and provide early warning of any serious degradation trends occurring in the propellant for service life predictions.

An analysis of all parameters indicates that no potential problems are expected in the propellant for at least two years past the oldest data point.

Data stored in the GO85 System were plotted utilizing the IBM 360-65 Computer and CAL-COMP Plotter. The data range at any age can be found by suitable inquiry of the GO85 System.

Each point on the regression plot represents the mean of all samples at that particular age. The number of specimens at each point is indicated on the sample size summary sheet accompanying each regression plot or group of regression plots.

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29A	Test Report (Missile in silo)	13 Jan 64
29В	Zero Time Test Results	29 Jan 64
29C	Zero Time Test Results (Supplement 1)	30 Mar 64
29D	Zero Time Test Results (Aft Closure)	9 Jun 64
29E	Zero Time (Aft Closure Supplement 1)	24 Jun 64
29F	ATP Phase I Test Results	30 Mar 65
29G	ATP Phase I Test Results	19 Aug 65
29Н	ATP Phase I Test Results	10 Sep 65
32A	Zero Time, Wings II-V Test Results	17 Mar 65
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49	ATP Phase I, Wings II-V (First Group)	18 Mar 66
53	ATP Phase I, Wings II-V (Second Group)	22 Apr 66
55	ATP Phase I, Wings II-V (Third Group)	29 Apr 66
58	ATP Phase I, Wings II-V (Fourth Group)	6 May 66
61	ATP Phase I, Wings II-V (Fifth Group)	10 Jun 66
66	ATP Phase I, Wings II-V (Sixth Group)	22 Jul 66
76	ATP Phase II, Wing I Test Results	24 Jan 67
78	Zero Time, Wing VI Test Results	3 Feb 67
104	ATP Phase I, Wing VI (First Group)	12 Oct 67
118	ATP Phase II. Wings II-V (First Group)	5 Mar 68

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Report Nr	<u>Title</u>	Repo	rt	Date
126	ATP Phase II, Wings II-V (Second Group)	11	Apr	68
130	ATP Phase II, Wings II-V (Third Group)	3	May	68
162	ATP Phase I, Wing VI (Second Group)	30	Sep	69
176	ATP Phase II, Wing VI (First Group)	15	Apr	70
181	ATP Phase III, Wing I	7	May	70
185	ATP Phase I, Wing VI (Third Group)	22	Jun	70
195	ATP Phase III, Wings II-V (Retest)	29	0ct	70
223	Surveillance Report LGM-30 Stage I (TP-H1011)		Sep	71
239	Surveillance Report LGM-30 Stage I (TP-H1011 and TP-H1043)		Apr	72
258	Surveillance Report LGM-30A & B Stage I, (TP-H1011)		Nov	72
268	Surveillance Report LGM-30A & B Stage I, (TP-H1011)		May	73
271	Surveillance Report LGM-30F & C Stage I, Phase A Series II, (TP-H1011)		Jul	73
277	Surveillance Report LGM-30F & G Stage I, Phase A Series III, (TP-H1011)		0ct	73
280	Surveillance Report LGM-30A & B Stage I, (TP-H1011)		Nov	73
288	Propellant Surveillance Report LGM-30A & B, Stage 1, TP-H1043		Mar	74
290	Propellant Surveillance Report LGM-30F & G, Stage 1, Phase B, Series I, TP-H1011		Mar	74
300	Minuteman Stage 1 Motor Reliability Improvement Program Surveillance		May	74

LIST OF REFERENCES (CONT)

Report Nr	<u>Title</u>	Report	Date
302	Propellant Surveillance Report LGM-30 A & B Stage 1, TP-H1011	Nov	74
313	Stage 1 Propellant Surveillance Report, Propellant Containing Glacial Acrylic Acid	Oct	74
315	Propellant Surveillance Report LGM-30 F & G Stage 1, TP-H1011	Jan	75
316	Propellant Surveillance Report LGM-30 A & B Stage 1, TP-H1011	Feb	75
319	Propellant Surveillance Report LGM-30 Dissected Motors, Phase VI, TP-H1011	Apr	75
321	Propellant Surveillance Report LGM-30 F & G Stage 1, Phase B, Series II, TP-H1011	Apr	75
325	Propellant Surveillance Report LGM-30 A & B Stage 1, TP-H1011	Jun	75
328	Propellant Surveillance Report LGM-30 A & B Stage 1, TP-H1011	Sep	75
330	Propellant Surveillance Report LGM-30 F & G Stage 1, TP-H1011	Oct	75
335	Stage 1 Motor Reliability Improvement Program	Dec	75
337	Propellant Surveillance Report LGM-30 A & B, Stage 1, TP-H1043	Feb	76
339	Stage 1, New MAPO & ERL-510 Qualification	Mar	76
341	Propellant Surveillance Report LGM-30	Mar	76

GLOSSARY OF TERMS AND ABBREVIATIONS

Aging Trend A change in properties or performance resulting

from aging of material or component

CSA Cross Sectional Area

DB Dogbone

Degradation Gradual deterioration of properties or performance

E Modulus (psi), defined as stress divided by strain

along the initial linear portion of the curve.

EB End Bonded

EGL Effective Gage Length

Strain at maximum stress em

er Strain at rupture

"F" ratio The ratio of the variance accounted for by the

> regression function to the random unexplained variance. The regression function having the most significant "F" ratio is used for plotting data. The ratio is also used in detecting signi-

ficant changes in random variation between

succeeding time points

JANNAF Joint Army, Navy, NASA, Air Force Committee

MANCP Propellant Lab Section at Ogden Air Logistics Center

Ogden ALC Ogden Air Logistics Center, Air Force Logistics

Command

r or R The Correlation Coefficient is a measure of the

degree of closeness of the linear relationship

between two variables

Linear The general form of the linear regression equation

is Y = a + bxRegression

Regression

Equation

Line representing mean test values with respect

Line to time

Standard error of estimate of the regression Sb

coefficient

CLOSSARY OF TERMS AND ABBREVIATIONS (cont)

Se or Sy.X Standard deviation of the data about the

regression line

Sm Maximum Stress

Sr Stress at rupture

Standard Square root of variance

Deviation (Sy)

Strain Rate Crosshead speed divided by the EGL

"t" test

A statistical test used to detect significant differences between a measured parameter and an expected value of the parameter (determines if regression slope differs from zero at the 95%

confidence level)

Variance The sum of squares of deviations of the test results from the mean of the series after division by one less than the total number of test

results

3 Sigma Band The area between the upper and lower 3 sigma limit. It can be expected that 99.73% of the inventory represented by the test samples would fall within this range assuming that the popu-

lation is normally distributed.

90-90 Band It can be stated with 90% confidence that 90% of

the inventory represented by the test samples would fall within this range assuming that the

population is normally distributed

INTRODUCTION

A. PURPOSE:

Quality assurance tests have been conducted for thirteen and one-half years on First Stage LGM-30A and B Minuteman Motor Propellant blocks to evaluate the effects of aging on TP-H1011 propellant.

Statistical analysis of the tests performed, as directed by Engineering, should provide early warning if serious degredation trends occur. Annual evaluation of the propellant provide data that can be directly input into engineering reliability and service life predictions. Testing was performed in accordance with MMEMP Directive GTD-1C and GTD-1C Amendments 1 and 2.

B. BACKGROUND:

Testing was first accomplished at MANCP on LGM-30A TP-H1011 propellant blocks in 1963 and was designated Zero-Time Testing (MAGCP Report Nrs 29B, 29C and 29F). Subsequent testing was accomplished at approximately 24 month intervals (MAGCP Report Nrs 29G, 29H - Phase I; 76 - Phase II; 181 - Phase III).

LGM-30B Zero-Time testing was accomplished in 1964 with subsequent testing at intervals of 24 months (MAGCP Report Nrs 32A-Zero-Time; 32C, 49, 53, 55, 58, 61, 66 - Phase I: 118, 126, 130 - Phase II; 195, 268 - Phase III).

Reports prior to MAGCP Report Nr 223(72) contained raw data

using sigma relation to compare to Zero-Time variance. MANCP Report Nr 239(72) published in April of 1972 contained all the data on LGM-30A, B, F and G in the GO85 System at that time. Report Nrs 258(72), 268(73), 280(73) reported LGM-30A and B data in statistical analysis by itself. This report is the sixth time that LGM-30A and B data have been reported in this manner.

Zero-Time testing was started as soon as possible after receipt of the propellant by MANCP. Data from these tests were used to establish a base line for each test to which each subsequent test data (ATP - Accelerated Test Plan) were compared in the reports listed above.

The LGM-30A and B propellant test matrix (Table 1) were used to determine the number of specimens to be taken from each propellant loaf and the specific test or tests to which these specimens were subjected. Low rate tensile and hardness specimens were taken from all LGM-30A and B blocks. Specimens for other physical and combustion tests were taken from every seventh block.

Some tests were not conducted at the earlier test periods (0-6 years) and, therefore, data are not available for inclusion in the regressions.

Table 1
Test Program

The test matrix is taken from GTD-1C, Amendment 2, and the tests, conditions, number of specimens and test methods are listed below.

Test	Conditions	Description	Per Cond
Hardness	10 Sec	Dogbone Ends	3
Low Rate Tensile	2.0 in/min	1/2" JANNAF Dogbone	3
High Rate Tensile	1750 in/min	3/4" Dogbone	3
High Rate Triaxial Tensile	600 psi, 1750 in/min	3/4" GL Rail End Bonded	1
Low Rate Biaxial Tensile	0.2 in/min	3/4" GL Rail End Bond	1
Stress Relaxation	3% & 5%	1/2" x 1/2" x 4" EB	3
Dynamic Response	70 gm ct wt	3.3" dia x .33" disc	1
Sol Gel		1/2" x 1/2"	8
VLR	2×10^{-3} in/min	1/2" JANNAF Dogbone	3
Ignitability	$168 \text{ cal/cm}^2 \text{ sec}$.050" wafer	3
TCLE		.200" wafer	3
Pressure Time	500 psi	1/2" x 3/8" x 1"	3
Burning Rate	1000 psi	.156" x .156" x 5" Strand	3
DTA	12°C Rise/min	.040" wafer	3
DSC		.040" wafer	3
Poisson's Ratio	77°F <u>+</u> 2° 15% Strain	.50" x .50" x 4"	6
Tear Energy	70°F ± 2°	0.1" x 1.18" x 3"	6
Failure Envelope		JANNAF Dogbone	3

STATISTICAL DISCUSSION

In order to determine aging trends for shelf/service predictions, regression analysis was selected as the method of data evaluation. In selecting the best fit model, eight models were tried. The linear model, Y = a + bX, was found to be the best fit for the regressions. By using the best fit model, the trend line becomes a more accurate predictor of future trend.

In some cases, the early test results show evidence of data biasing due to considerable changes which are probably post-cure effects of the propellant during the first few years. These post-cure effects tended to skew and produced unrealistic data trend lines. In these cases, data trends were analyzed starting at six years of age where the trend lines were no longer affected by post-curing of the propellant.

Individual data points from different time periods were pooled to establish a least squares trend line for the data. The variance about the regression line, obtained using individual values of the dependent variable, was used to compute a tolerance interval such that at the 90% confidence levl 90% of the sample distribution falls within this interval. This tolerance interval was extrapolated to a maximum of 24 months into the future from age of the oldest sample tested. The 't' values and the significance of this statistic, which are reported for each regression model, give an indication of the "statistical significance" of the slope of the trend line as compared to a line of zero slope. Data were plotted by computer. The "y" axis is computed so

that the values at one inch intervals are peculiar to the data spread of the parameter tested. Plotted data points represent means at the particular ages at which testing occurred. The number of specimens at each age point is indicated on the sample size summary sheet accompanying each regression plot. Variance at each test age can be determined by consulting the GO85 data storage system.

TEST RESULTS

A. TENSILE

Regressions for very low rate tensile data show a statistically significant decrease for strains and both stresses with a statistically significant increase for modulus (Figures 1 thru 5).

The low rate tensile for both strains and stress at rupture show a statistically significant decrease while maximum stress show no significant aging trend. Modulus shows a statistically significant increase (Figures 6 thru 10).

Low rate biaxial tensile shows a statistically significant decrease for strain at rupture, and a statistically significant increase for modulus. There were no significant changes in the other parameters (Figures 11 thru 15).

The high rate tensile strain at maximum stress, stress at rupture and modulus show a statistically significant increase. Strain at rupture shows a statistically significant decrease. Maximum stress shows no aging trend (Figures 16 thru 20).

For triaxial tensile testing, strain at maximum stress shows a statistically significant increase. Strain at rupture and both stresses show no change. The modulus shows a statistically significant decrease (Figures 21 thru 25).

In general, the regressions for all of the tensile testing show trends that are gradual and no operational problems are expected for at least two years beyond the oldest data point.

B. STRESS RELAXATION:

Modulus at 3% and 5% strain shows a statistically significant increase at all time periods (Figures 26 thru 33). However, the trend lines are gradual and no operational problems are expected.

C. HARDNESS:

The propellant shows a statistically significant increase in hardness. This increase is gradual as indicated by the slope of the curve which is close to a line of zero slope (Figure 45).

D. DYNAMIC RESPONSE:

The storage shear modulus at 200 and 400 hz shows a statistically significant decrease, while loss tangent at 200 and 400 hz shows a statistically significant increase (Figures 35 thru 38).

E. PRESSURE TIME:

A statistically significant increase is shown in time to maximum pressure with the maximum pressure showing a statistically significant decrease (Figures 39 and 40).

F. TCLE: (Thermal Coefficient of Linear Expansion)

The thermal coefficient of linear expansion below and above the glass transition point shows a statistically significant increase. In both cases the increase is gradual (Figures 41 and 42).

G. DSC: (Differential Scanning Calorimeter)

The first endotherm peak temperature (on this propellant there is only one endotherm) shows a statistically significant increase; the first and second exotherm peak temperature shows no change. (Figures 43 thru 45).

H. IGNITABILITY:

No significant change is seen in this parameter (Figure 46).

1. BURNING RATE:

A statistically significant decrease is shown; however, the decrease is gradual and no problems are forseen for at least two years past the last data point (Figure 47).

J. SOL GEL:

A statistically significant decrease is shown for weight swell ratio and percent extractables. The cross link density shows a statistically significant increase (Figures 48 thru 50).

The increase in cross link density correlates well with the decreasing strain (elasticity), increasing stress, modulus and hardness trends.

CONCLUSIONS

This report includes LGM-30 A and B bulk propellant test results presently in the GO85 System and covers the past thirteen and one-half years of testing.

The test results show that under present storage conditions the physical/mechanical and combustion properties of the propellant are remaining relatively stable with age. This is indicated by the regression plots where the slope of the trend line is relatively flat or close to a line of zero slope and have not changed appreciably from the last test period.

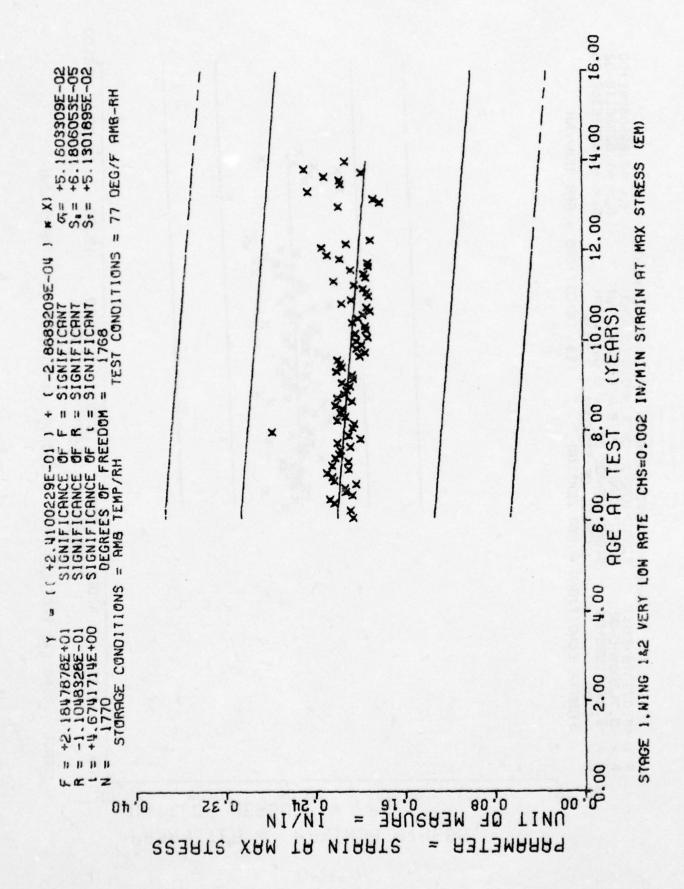
From the statistical analyses, all tests conducted indicate that motor propellant reliability will not be affected for two years past the last data point on the regression.

*** SAMPLE SIZE SUMMARY ***

S) SAMPLES	9	9	9	-	3		•																		
(MONTHS)	160.0	162.0	163.0	164.0	165.0	166.0	168.0									-									
SAMPLES	18	15	56	45	28	18	25	24	20	39	45	18	36		12	- \$2	33	- 13	9		3		2	+	3
(MONTHS)	125.0	126.0	127.0	128.0	129.0	136.0	131.0	132.0	133.0	1340	135.0	136.0	137.0	136.0	139.0	140.0	141.0	142.0	143.0	145.0	146.0	147.0	156.0	157.6	158.0
SAMPLES	34	45	34	- 69	50	36	23		44	-61	56	- 24	59	4.	15	16	27		33		36	- 54	21	- 61	20.
(MONTHS)	130.0	10101	102.0	1.08.41	134.3	10501	106.0	157.0	108.0	169.0	110.0	111.	112.0	113.0	114.0	1150	116.0	117.	118.3	119.0	126 •0	121.3	122.0	1230	124.0
SAMPLES	5	18	81	-	0	135	18		1.8	- 81	C	4.5	27	- 63	13		36	t	15	- 66	2.5	- 63	34		33
(MONTHS)	736.0	15.0	77.0	780	20.62	A30	81.0	82.0	83.0	94.6	85.0	6.98	87.0	6.98	83.0	6366	61.0	92.0	93.0	0.00	95.0	96.0	0.26	- 686	0.66

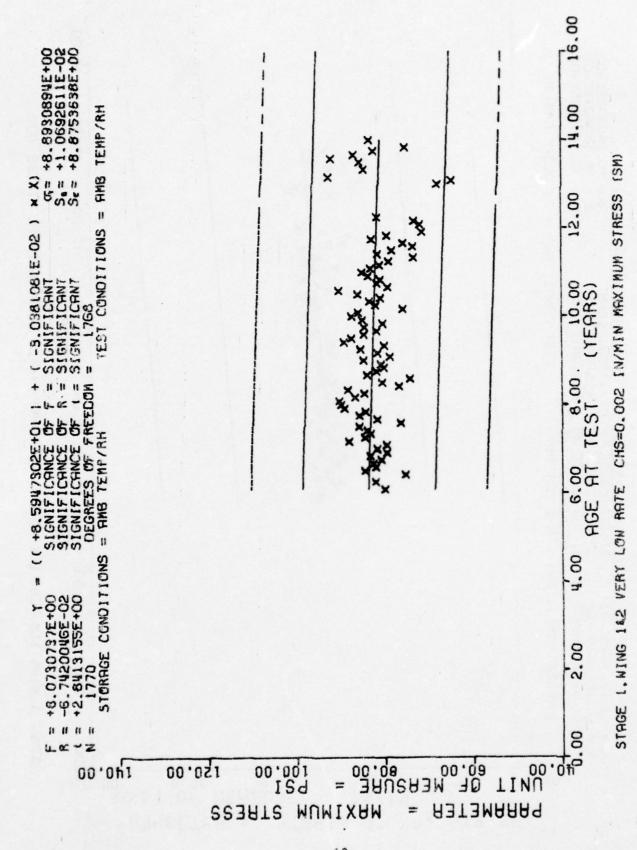
STAGE 1941NG 162 VERY LOW RATE CHS=0.002 IN/MIN

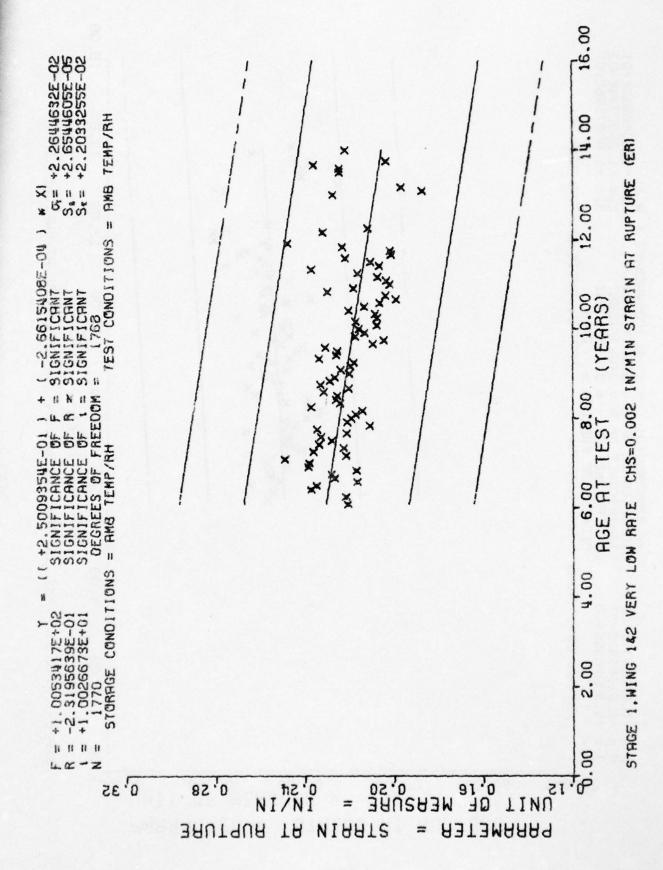
This sample size summary is applicable to figures 1 thru 5.

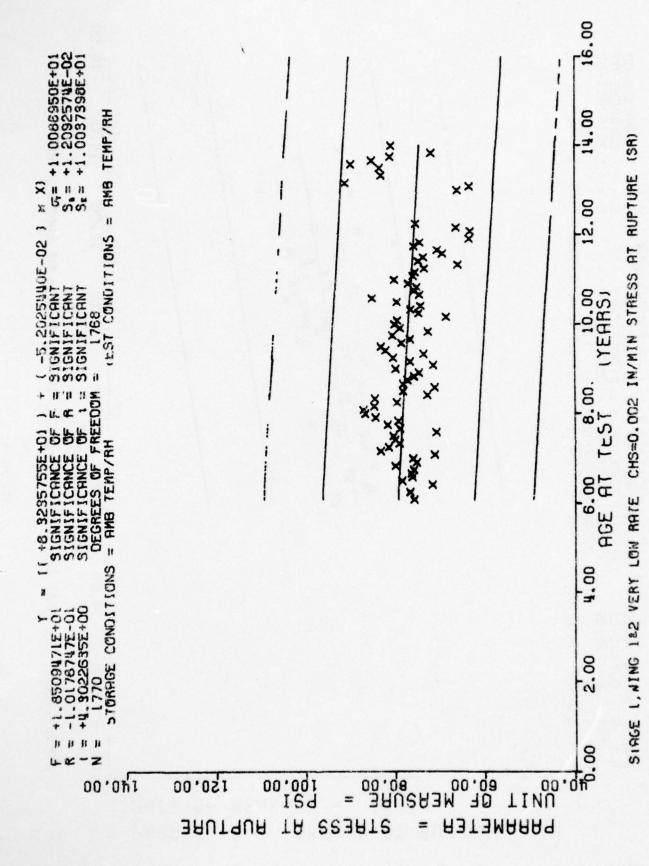


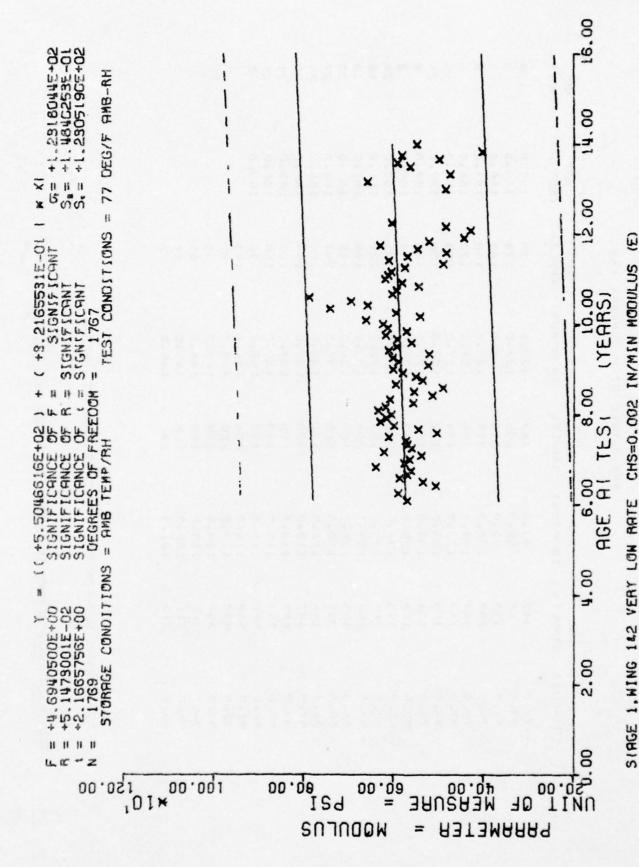
_ 11 -

Figure









- 15 -

*** SAMPLE SIZE SUMMARY ***

(MINTHS)	MA	AGE	77	Arst	27.	AGF	an
	SAMPL ES	(MONTHS)	SAMPLES	(MONTHS)	SAMPLES	(MUNTHS)	SAMPLES
72.0	142	0.79	143	122.0	75	147.0	39
73.0	66	0.86	235	123.0	174	148.0	8
74.0	133	0.06	215	124.0	160	150.0	8
75.0	585	100.0	519	125.0	198	151.0	9
76.0	147	101.0	186	126.0	170	154.0	C.
77.0	157	102.0	174	127.0	183	156.0	15
78.0	153	103.0	177	128.0	156	157.0	24
79.0	134	1 04 .0	151	129.0	183	158.0	6
80.0	194	105.0	217		160	159.0	10
81.0	153	106.0	274	131.0	161	160.0	24
82.0	26.0	107.0	153	132.0	221	161.0	15
83.7	166	108.0	254	133.0	158	162.0	12
34.0	183	139.0	182		215	163.0	39
85.0	307	110.0	165	135.0	281	164.0	27
86.0	144	1111.0	171	136.0	264	165.0	24
87.0	467	112.0	322	137.0	198	166.0	30
33.0	682	113.0	155	138.0	135	167.0	21
80.0	783	114.0	213	139.0	168	168.0	21
9.06	905	1.15.0	193	140.0	92	169.0	5
0.10	558	116.0	204	141.0	193		
92.0	527	117.0	220	142.0	46		
03.9	262	118.0	228	143.0	33		
04.0	365	119.0	162	144.0	45		
0.50	311	120.0	188	145.0	27		
0.90	- 212	121.9	238	146.0	3		

STAGE 1. WING 162 LOW RATE TENSILE CHS=2.0 IN/MIN

This sample size summary is applicable to figures 6 thu 9.

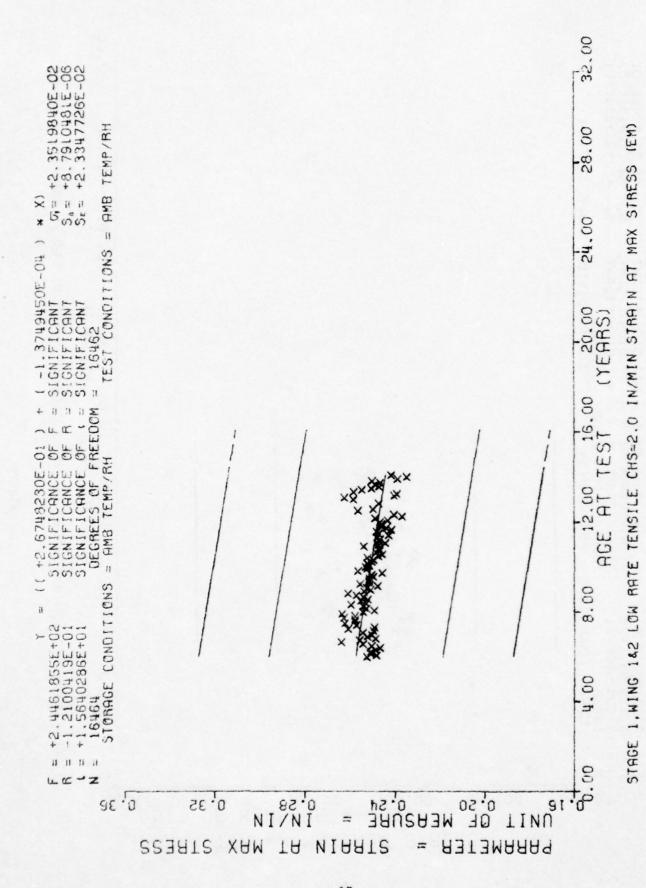
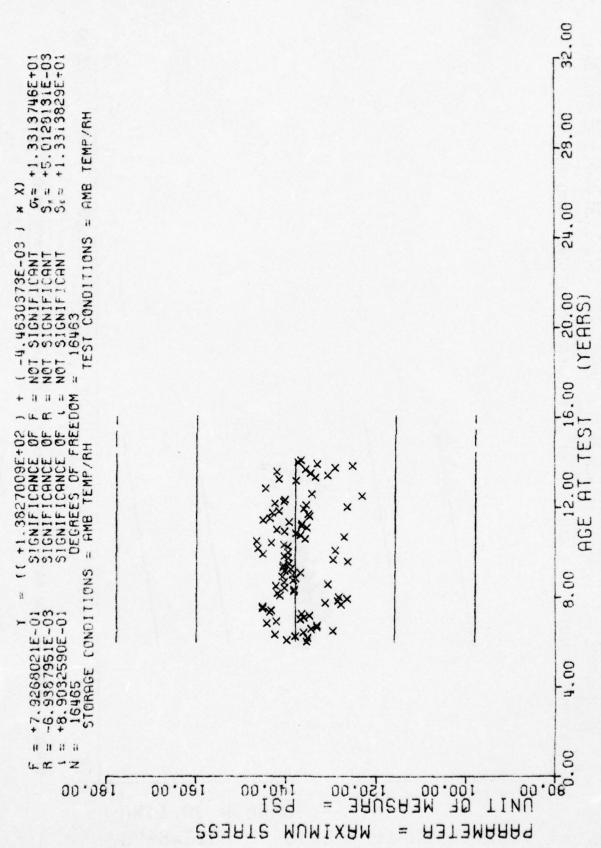
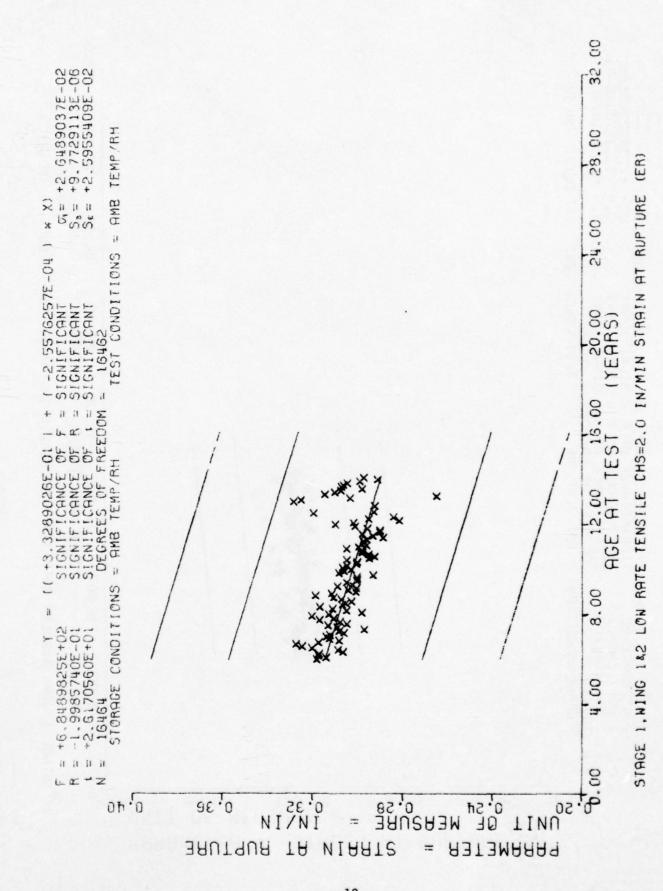


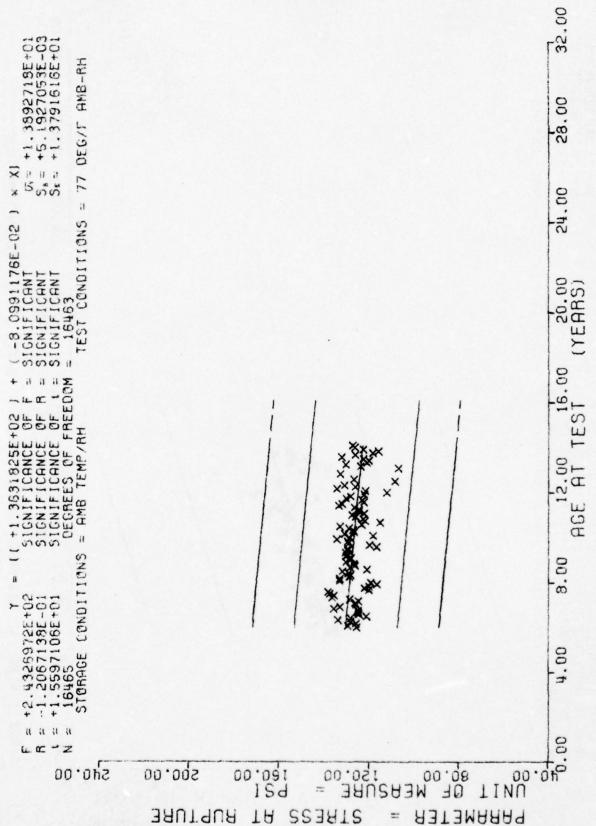
Figure 6



STAGE I, WING 142 LOW RATE TENSILE CHS=2.0 IN/MIN MAXIMUM STRESS

(SM)





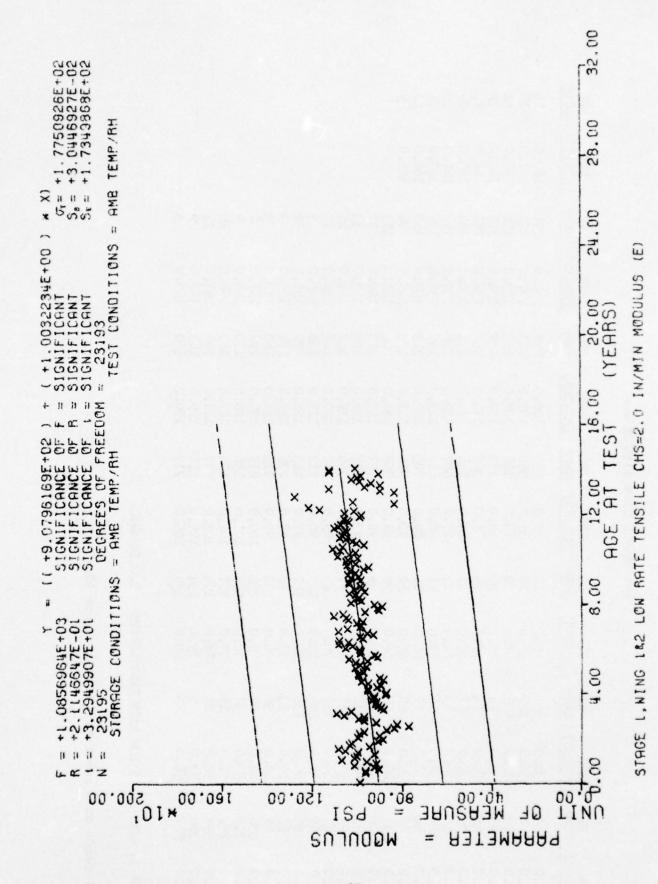
STAGE 1, WING 142 LOW RATE TENSILE CHS=2.0 IN/MIN STRESS AT RUPTURE (SR)

Figure 9

SAMP	28282382482 28282382482
AGE (MONTHS)	160.0 161.0 163.0 164.0 165.0 168.0 168.0
SAMP	44844884888888888888888888888888888888
AGE (MONTHS)	133.00 13
SAMP	663 453 453 882 822 453 853 853 853 853 853 853 853 853 853 8
AGE (MONTHS)	106.0 109.0 111.1 109.0 112.1 112.0 123.0 123.0 123.0 123.0
SAMP	12118368755388388877 121183687553887888788877
AGE (MONTHS)	88 88 88 88 88 88 88 88 88 88 88 88 88
SAMP	######################################
AGE (MONTHS)	87777777777777777777777777777777777777
SAMP	~ ~ 5 6 7 3 8 7 8 7 8 7 8 7 8 8 3 8 8 3 8 8 7 8 7 8 8
AGE (MONTHS)	84484848883444444444444444444444444444
SAMP	いなどないないないないないないのではないないできることできることできることできることできることできることできることできること
AGE (MONTHS)	28 28 28 28 28 28 28 28 28 28 28 28 28 2

STAGE 1, WING 1 & 2 LOW RATE TENSILE CHS = 2.0 IN/MIN

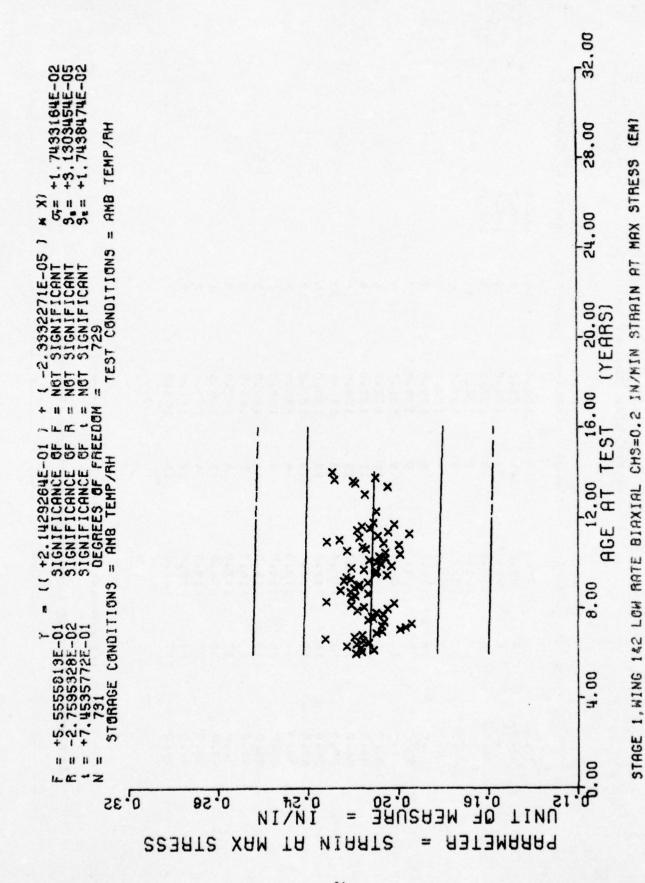
This sample size summary applies to figure 10.

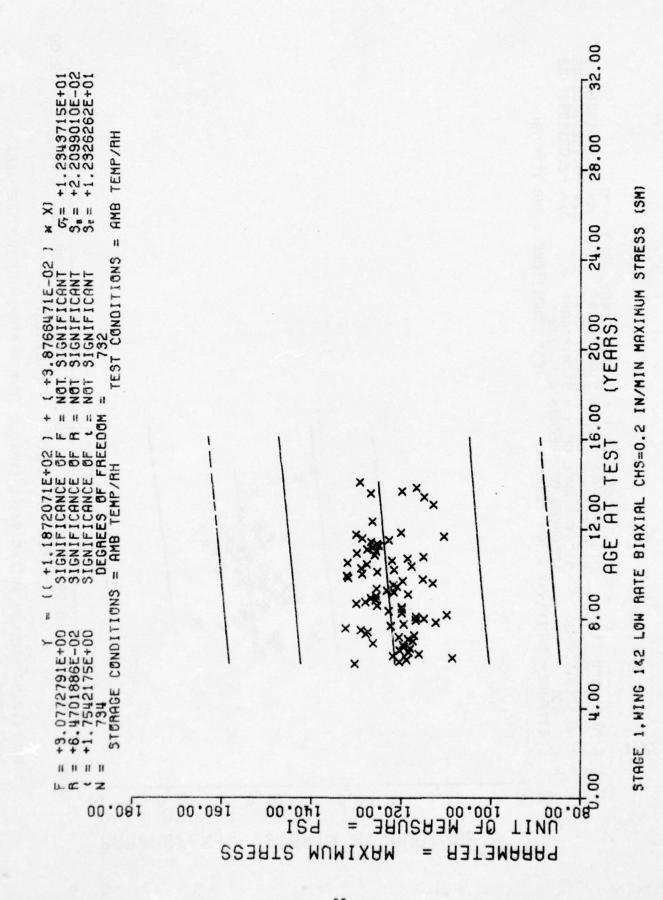


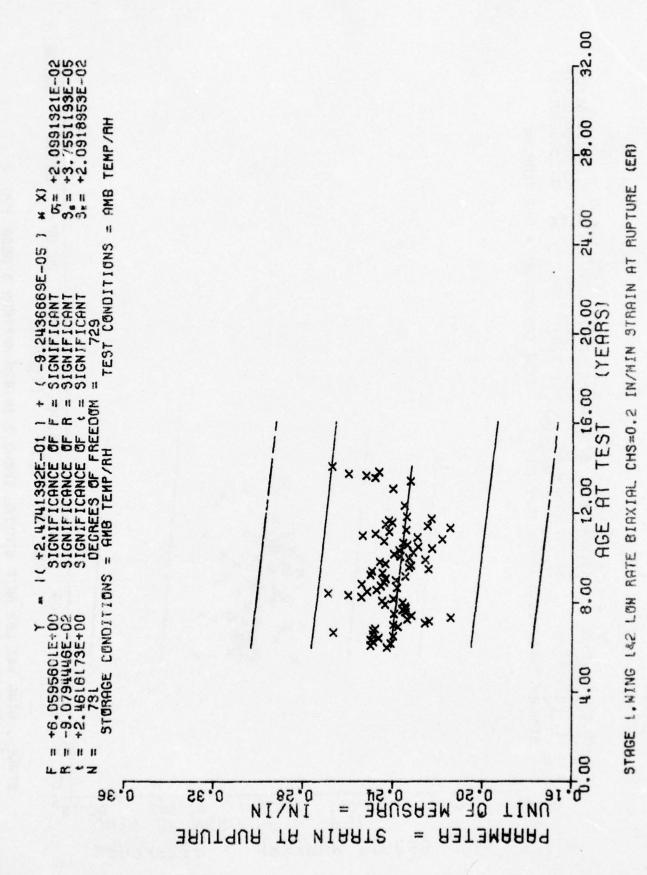
N. C.	SAMPLES	Ю	•	6	1						And the second of the second of the second															
AGE	(MONTHS)	164.0	165.0	166.0	169.0																					
αZ	SAMPLES	16	9	13	6	11	9	α	1	1	4	4	4	9	13	91	10	œ	1	~	6	S		~	2	-
AGE	(MONTHS)	122.0	123.0	124.0	125.0	126.0	127.0	128.0	129.0	130.0	131.0	132.0	133.0	134.0	135.0	136.0	137.0	138.0	130.0	140.0	141.0	142.0	148.0	157.0	161.0	163.0
ž	SAMPLES	O	-	m	S	2	4	4	6	6	6	10	11	12	60	12	-10	œ	9	11	. 2	80	u)	4	12	11
AGE	(MINTHS)	97.0	0.86	0.66	100.0	101.0	102.0	103.0	104.0	105.0	106.0	107.0	108.0	109.0	110.0	1111.0	112.0	113.0	114.0	115.0	116.0	117.0	118.0	119.0	120.0	121.0
αχ	SAMPLES	ю	6	4	c	C	12	7	16	5	10	15	13	. 11	11	18	-11	14	26	34	23	37	3.0	50	111	10
A GF	(MUNTHS)	72.0	73.0	74.0	75.0	76.0	77.9	78.0	79.0	80.0	81.0	82.0	83.0	84.0	85.0	86.0	87.0	38.0	89.0	0.00	91.0	92.0	93.0	0.46	95.0	0.95

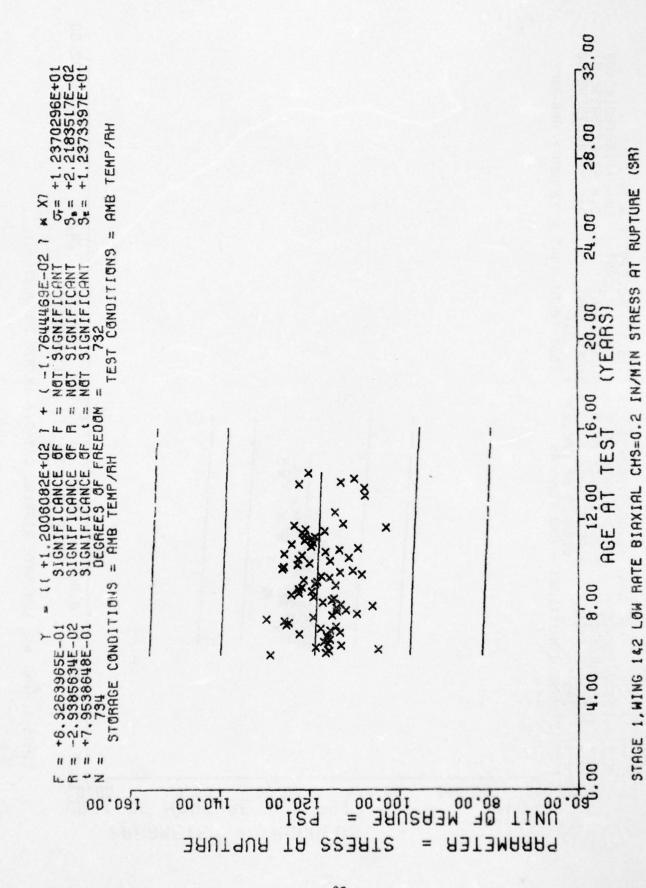
STAGE I.WING 182 LOW RATE BIAXIAL CHS=0.2 IN/MIN

This sample size summary is applicable to figures 11 thru 15.

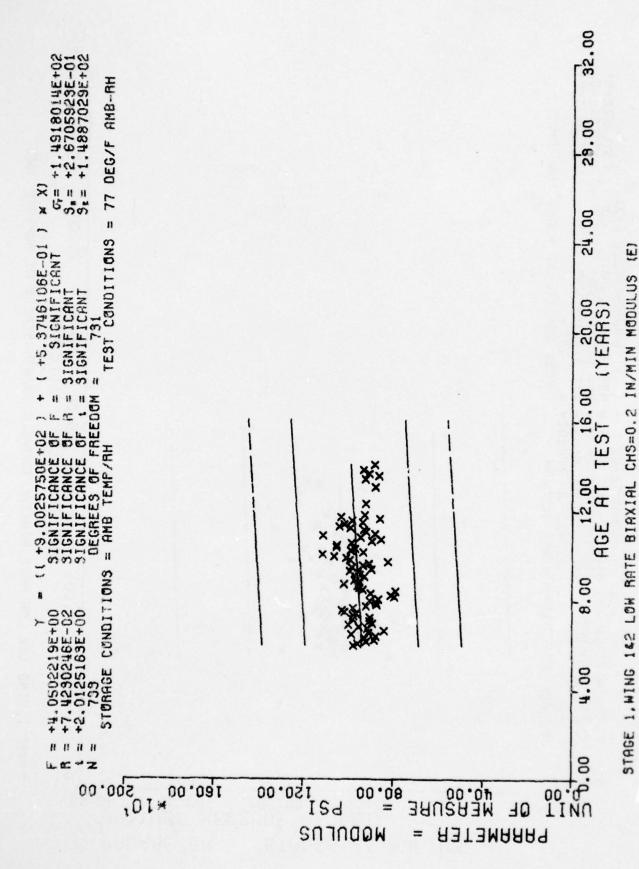








- 27 -



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*** SAMPLE SIZE SUMMARY ***

SAMPLES	36	30	σ	30	21	38	12	18	15	18	36	27	14	36	37	54	53	21	27	-11	6	13	17	9	
(MONTHS)	122.0	123.0	124.0	125.0	126.0	127.0	128.0	120.0	130.0	131.0	132.0	133.0	134.0	135.0	136.0	137.0	138.0	139.0	140.0	141.0	142.0	143.0	•	146.0	
SAMPLES	26	54	20	15	18	18	20	42	27	33	18	18	23	36	52	20	48	56	18	35	25	91	43	42	21
(MONTHS)	97.0	0.86	0.66	100.0	101.3	102.0	103.0	104.0	105.0	106.9	107.0	108.0	100.1	110.0	1111.0	112.7	113.0	114.0	115.0	116.0	117.0	118.3	119.0	120.0	121.0
SAMPLES	21	24	12	1.8	o	45	18	36	27	21-	63	24	36	22	20	69	101	- 75	85	99		64		42	
(MUNTHS)	72.0	73.0	74.0	75.0	76.0	77.0	78.0	79.0-	80.0	81.0	82.0	83.0	84.6	85.	96.0	87.0	88.0	69.0	0.06	01.0	05.0	93° u	0.40	05.0	0.96

STAGE 1. WING 182 HIGH RATE CHS=1

CHS=1750 IN/MIN

This sample size summary is applicable to figures 16 thru 20.

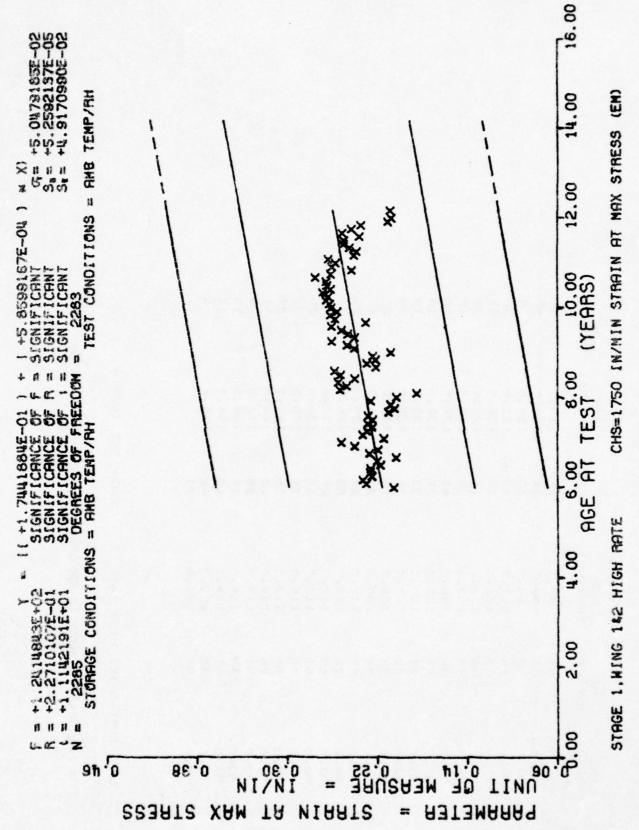


Figure 16

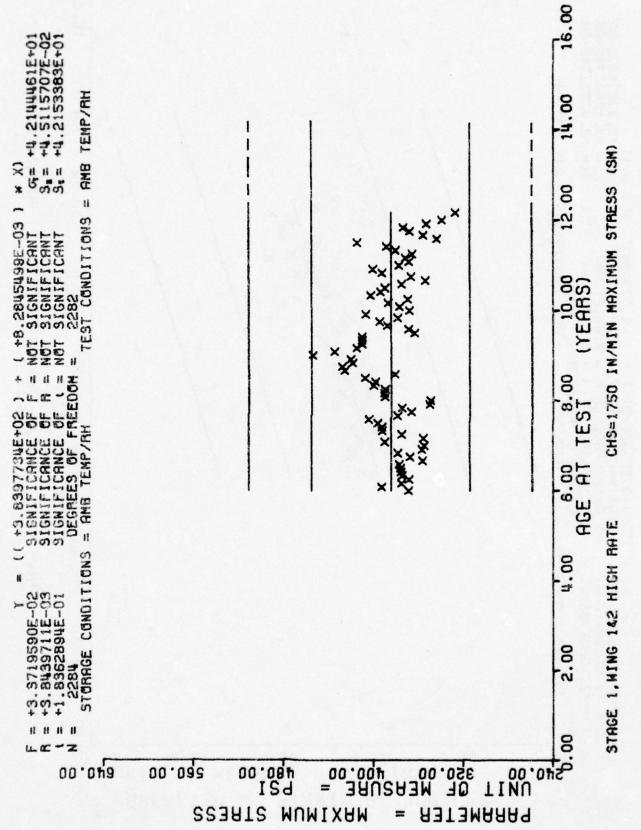
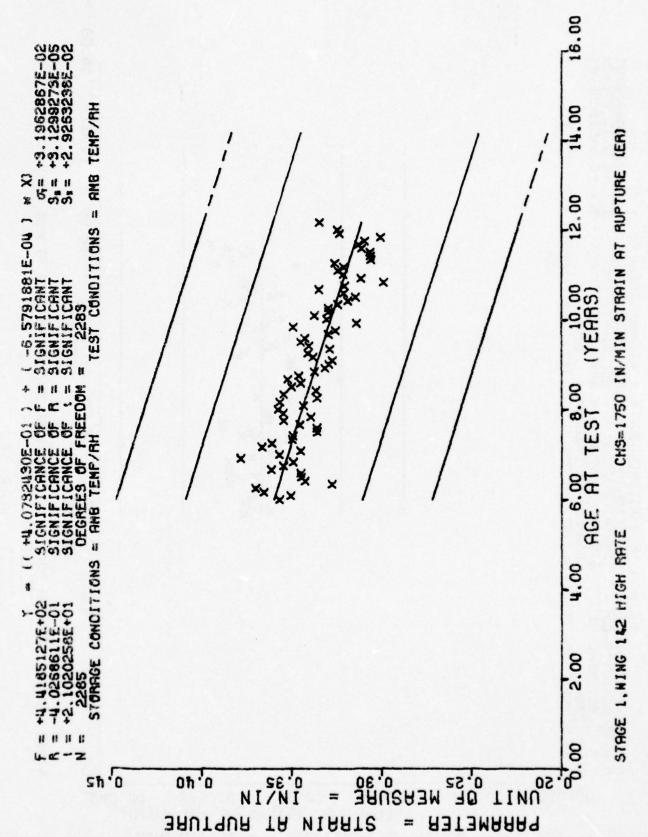


Figure 17



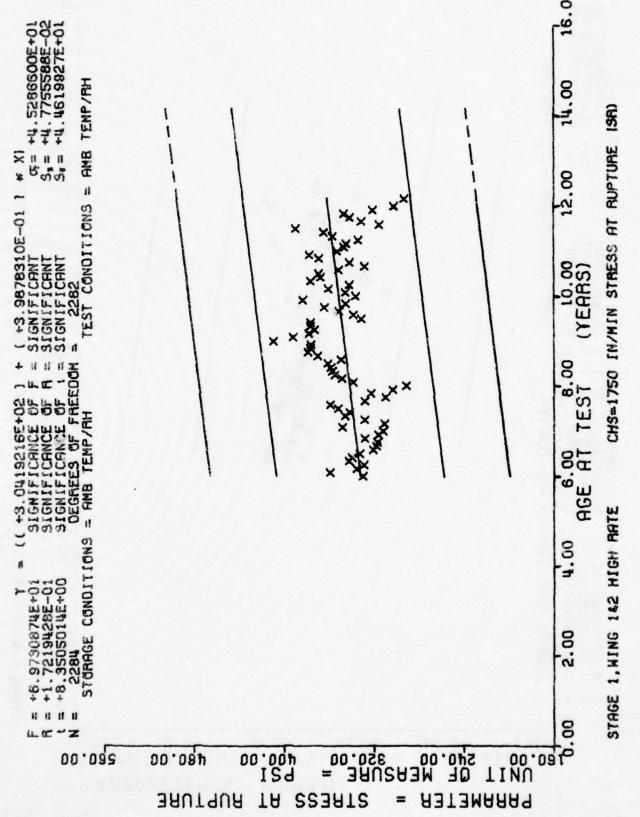
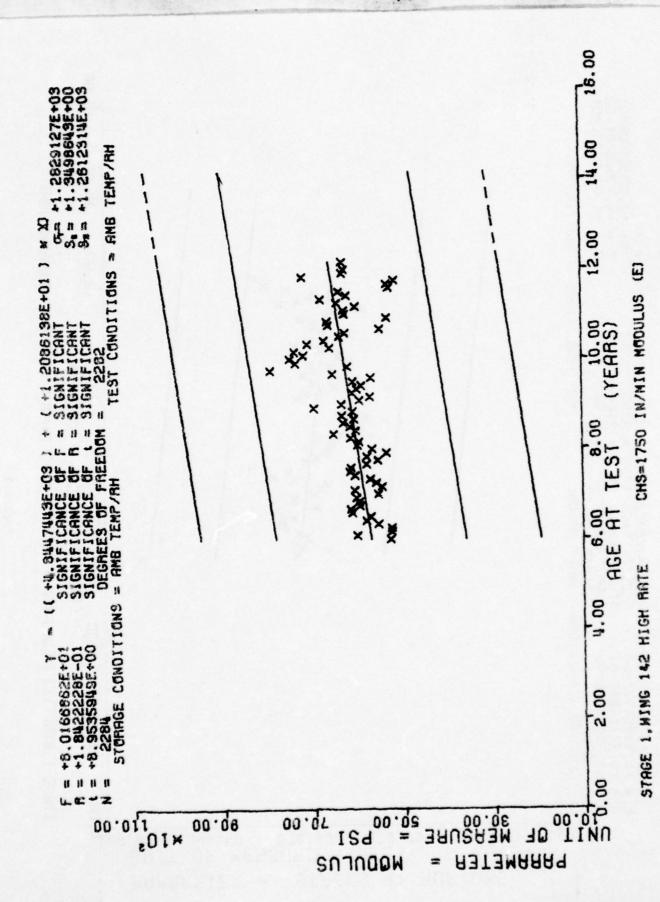


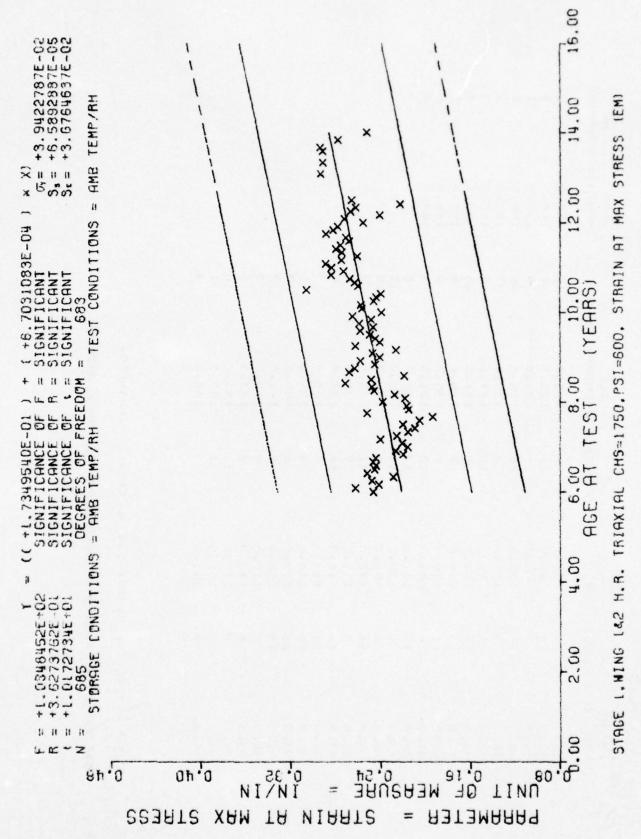
Figure 19

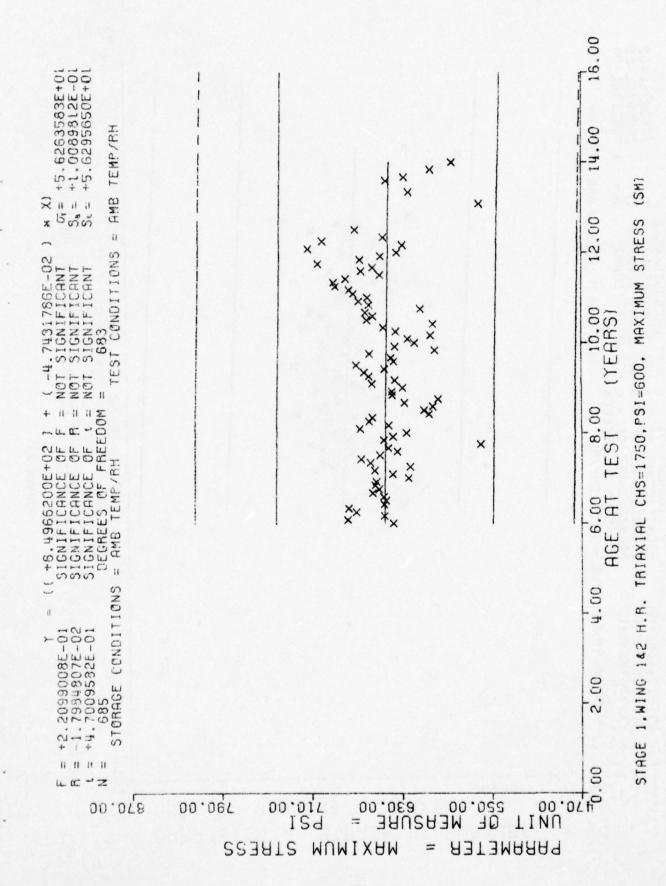


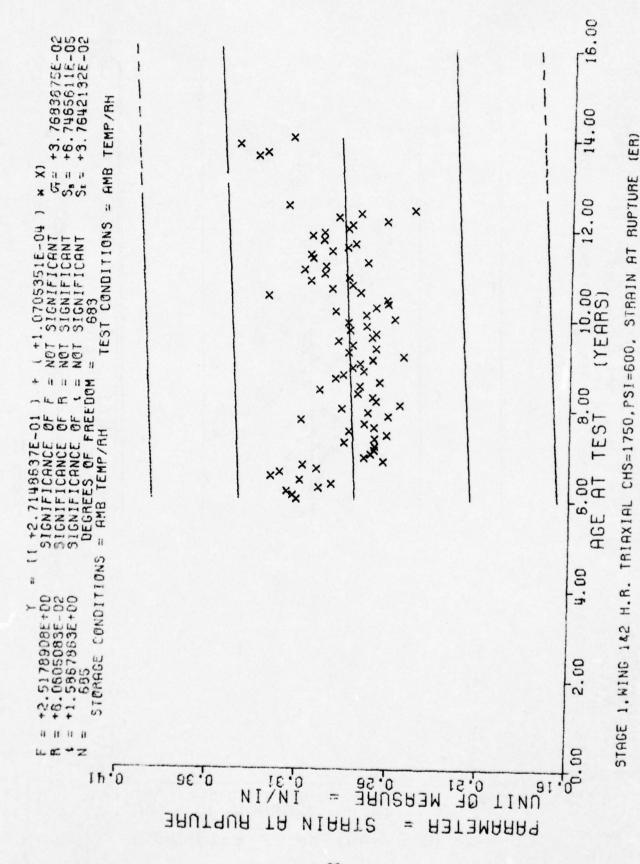
XX	SAMPLES	2		-	8	•	2	2	-	2				1			A A CANADA A CANADA A CANADA A CANADA									A
AGE	(MONTHS)	147.0	148.0	149.0	150.0	157.0	160.0	163.0	164.0	166.0	168.0															
× Z	SAMPLES	15	9	6	- 16	3	7	10	80	7	2	œ	12	12	2	8	9	m	5	3	r	2	2	10	-	6
A GE	(MONTHS)	122.0	123.0	124.0	125.0	126.0	127.0	128.0	129.0	130.0	131.0	132.0	133.0	134.0	135.0	136.0	137.0	138.0	1 39 • 0	140.0	141.0	142.0	143.0	144.0	145.0	146.0
Ž	SAMPLES	8	18	10	10	8	10	3	7	7	. 12	13	14	8	12	~	14	7	G	9	C	8	Ó	11	11	6
AGE	(MONTHS)	0. 70	98.0	0.66	100.0	101.0	102.0	103.0	104.0	105.0	106.0	107.0	138.0	100.0	110.0	111.0	-112.0	113.0	114.0	115.0	116.0	117.0	118.0	119.0	120.0	121.0
7	SAMPLES	σ	4	1	17	S	o	16	r)	1.1	4	13	7	7	15	5	14	21	25	98	13	S	9	α	6	œ
# C2	(MUNTHS)	72.0	73.0	74.0	75.0	76.0	0.77	78.0	79.0	80.0	81.0	82.0	83.0	84.9	95.0	86.0	87.0	33.0	89.0	0.06	91.0	92.0	93.0	0.40	95.0	0.96

STAGE 1.WING 162 H.R. TRIAXIAL CHS=1750, PSI=600,

This sample size summary is applicable to figures 21 thru 25.







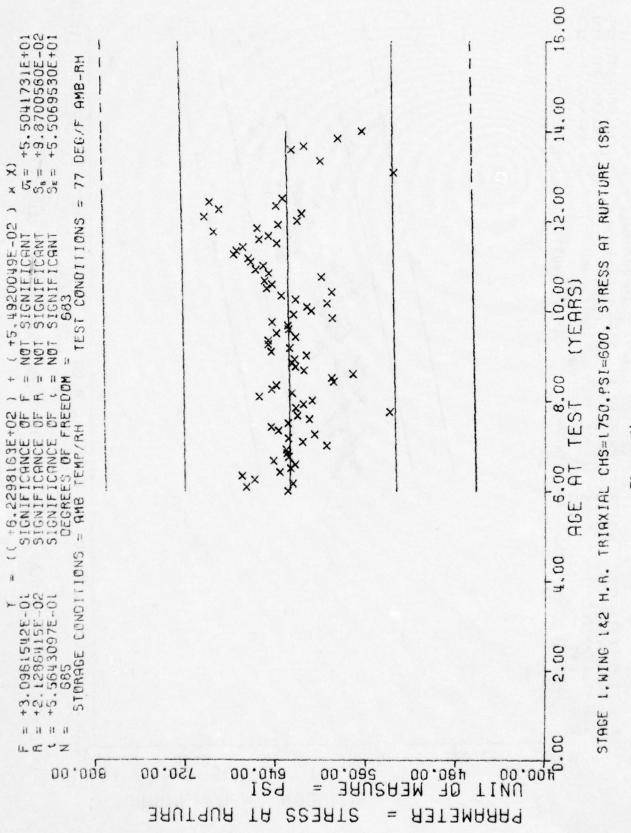
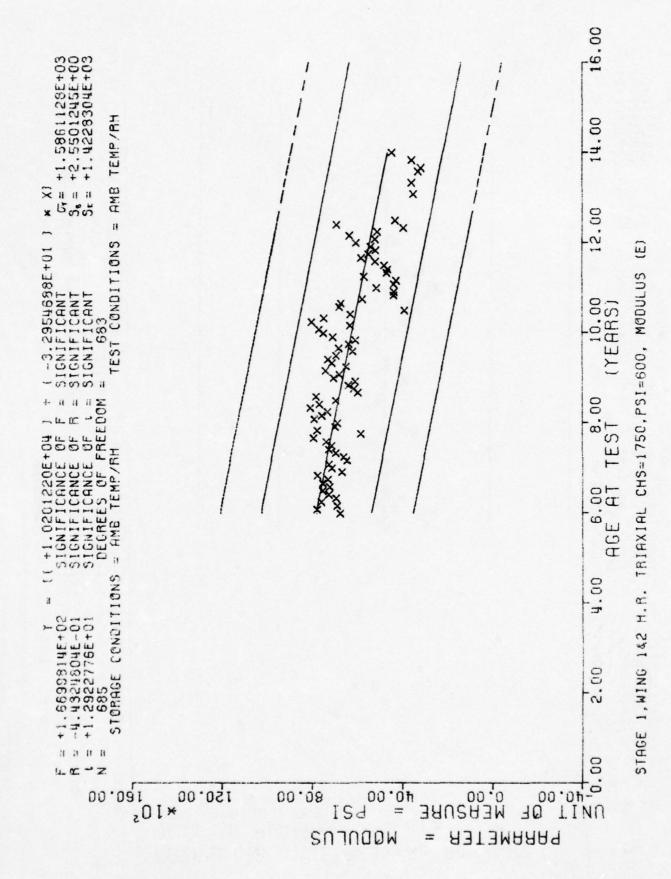
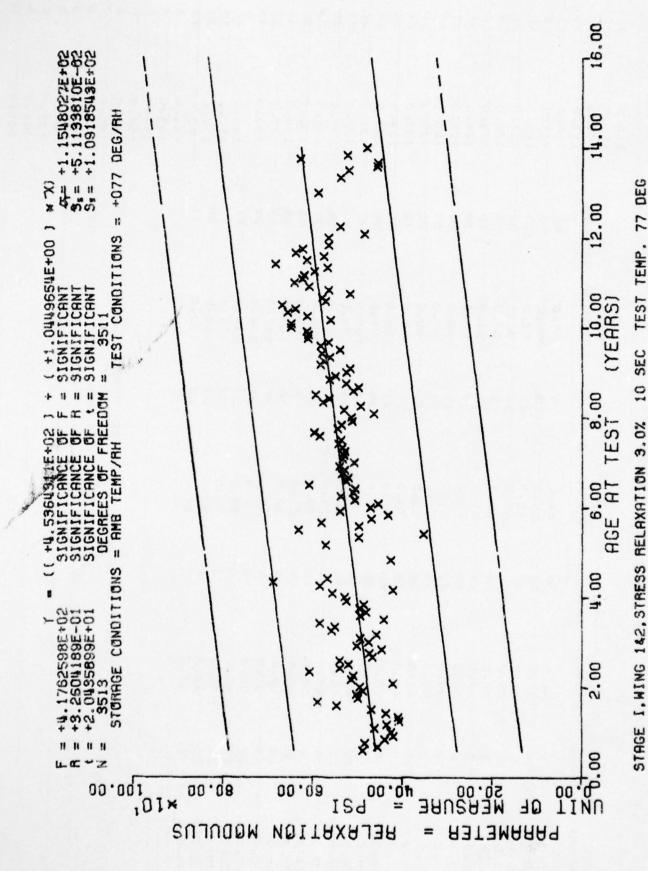


Figure 24



	And in case of	The second secon	and the property and the property of the property of the party of the	and the second s	The same of the sa		Company of the Control of the Contro		
								114.0	33
AGE	NR	AGE	MR	AGE	XX.	AGE	NR	115.0	36
(MONTHS)	SAMPLES	(MONTHS)	SANDLES	(MONTHS)	SAMPLES	(MONTHS)	SAMPLES	116.0	20
	And the second s	and the second s						117.0	35
7.0	4	32.0	36	64.0	6	89.0	99	118.0	21
8.0	3	33.0	38	55.0	12	0.06	72	119.0	36
0.6	3	34.0	30	0.99	23	91.0	113	120.0	42
10.0	4	35.0	- 59	67.0	24	92.0	63	121.0	15
11.0	S	36.0	59	68.0	9	93.0	93	122.0	0
12.0		37.0	23	0.69	17	94.0	99	123.0	12
13.0	9	38.0	50	70.0	27	95.0	36	124.0	27
14.0	10	39.0	22	71.0	24	0.96	30	125.0	21
15.0	12	40.0	28	72.0	24	0.76	23	126.0	44
16.0	6	41.0	38	73.0	13	98.0	30	127.0	15
17.0	9	42.0	84	74.0	21	0.66	15	128.0	21
18.0	8	43.0	63	75.0	21	100.0	48	129.0	33
	7	44.0	20	76.0	30	101.0	36	130.0	18
20.0	11	45.0	39	77.0	15	102.0	- 27	131.0	12
0.12	12	46.0	48	78.0	27	163.0	43	132.0	28
22.0	6	47.0	36	79.0	27	104.0	34	133.0	18
23.0	80	48.0	15	80.0	30	105.0	27	134.0	33
24.0	8	0.64		81.0	18	106.0	33	135.0	36
25.0	18	20.0	2	82.0	36	107.0	24	136.0	39
26.0	13	51.0	*	83.0	12	108.0	33	137.0	33
27.0	17	52.0	3	84.0	27	109.0	27	138.0	15
28.0		53.0	5	85.0	33	110.0	- 13	139.0	27
29.0	56	58.0	3	86.0	33	111.0	18	140.0	18
30.0	62	62.0	3	87.0	69	N	36	141.0	33
31.0	21	63.0	В	88.0	69	113.0	21	142.0	15
	The second secon	And the second s				sufficiently for the country of the	Management about the set that, general and definition of factors of factors and the set of the set	144.0	6
								145.0	3
			The same about the same of the					147.0	9
								155.0	5
STAGE I.	MING 182,5	STAGE ISMING 182, STRESS RELAXATION	ATTEN 3.0X		TEST TEMP.	י נו מבני		158.0	n
							An experience of selection of the contract of	160.0	6
This sample	le size summary	ary is applicable	100	figures 26 thru	29.			162.0	•
							The state of the s	163.0	F
			The state of the s					164.0	E
								165.0	9
								166.0	9



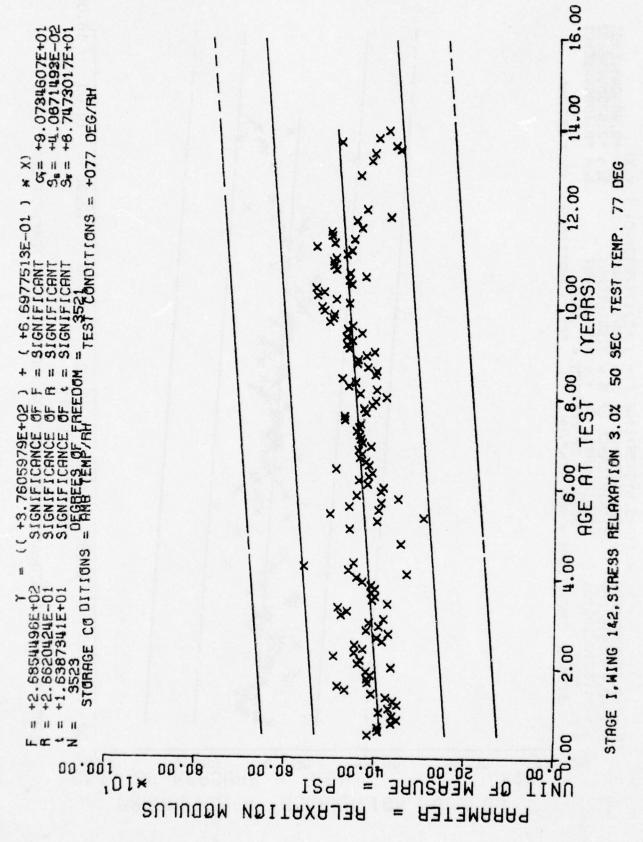
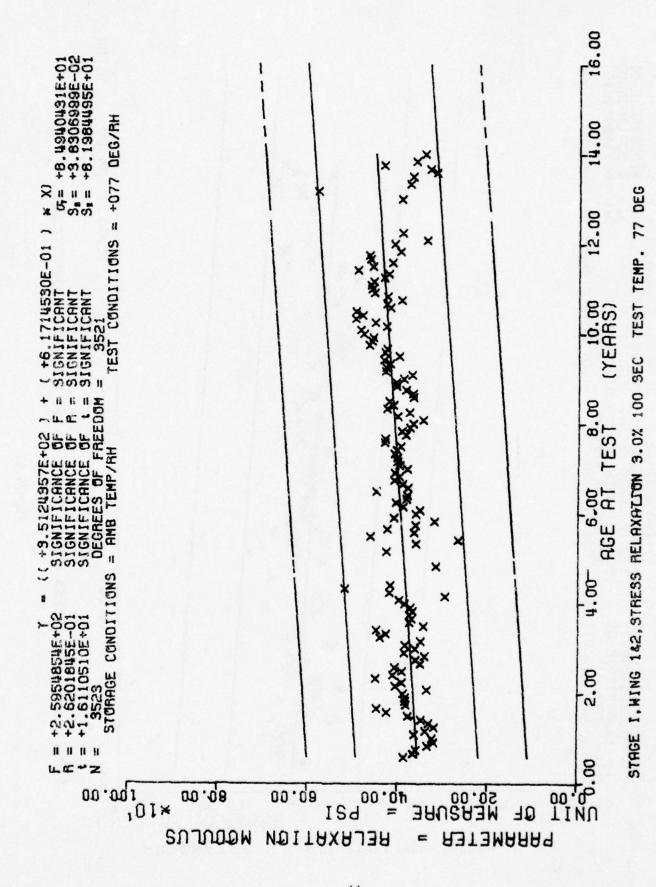
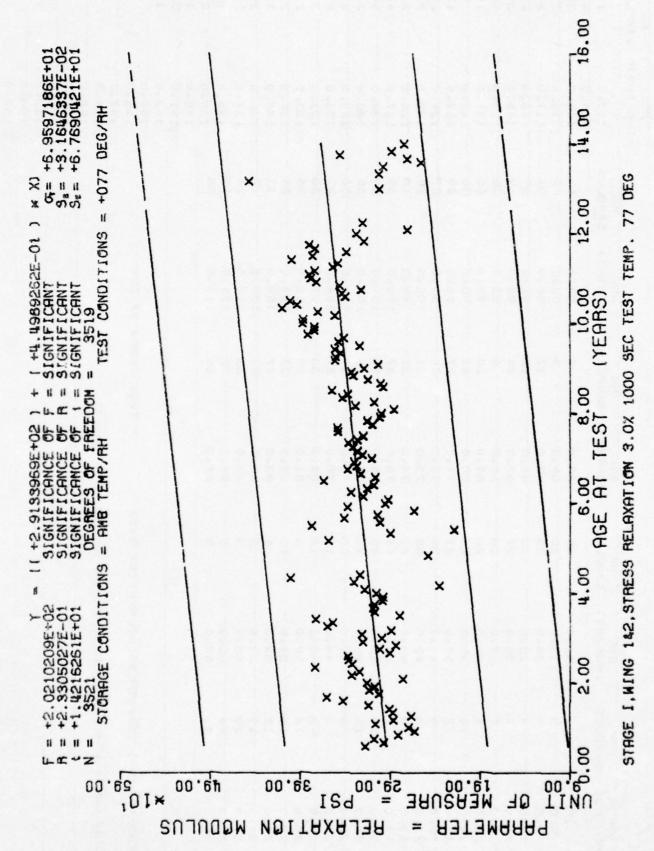


Figure 27





*		-
	1000	
	1	7
	-	The same of the sa
	8 6 6	*

7.0 7.0 8.0 9.0								COL NOW	SAMPLES
0.0	SAMPLES	(MONTHS)	SAMPLES	(MONTHS)	SAMPLES	(MONTHS)	SAMPLES	113.0	18
9.0					the second secon			114.0	33
0.6	4	32.0	90	63.0	m	88.0	99		30
0.6	3	33.0	38	64.0	6	89.0	69	116.0	12
10.0	S	34.0	30	65.0	12	0.06	81	117.0	39
	-	35.0	30	0.99	12	91.0	56	118.0	12
11.0	S	36.0	27	67.0	24	95.0	69	119.0	36
12.0		37.0	26	68.0	9	93.0	06	120.0	42
13.0	9	38.0	50	0.69	18	94.0	9	121.0	15
14.0	10	39.0	23	70.0	27	95.0	36	122.0	6
15.0	12	40.0	27	71.0	27	0.96	30	123.0	12
16.0	-	41.0	38	72.0	26	97.0	- 43	124.0	24
17.0	9	42.0	80	73.0	21	98.0	30	125.0	27
18.0	8	43.0	19	74.0	- 13	0.66	18	126.0	33
19.0	1	44.0	*	75.0	27	100.0	39	127.0	44
20.0	11	45.0	40	76.0	38	101.0	39	128.0	0#
21.0	12	46.0	48	77.0	15	102.0	30	129.0	21
6.23	6	47.0	36	78.0	- 27	103.0	36	130.0	72
23.0	80	48.0	15	19.0	27	104.0	27	131.0	27
24.0	8	49.0	17	80.0	30	105.0	38	132.0	33
25.0	18	20.0	2	81.0	50	106.0	36	133.0	21
26.0	13	51.0	13	82.0	33	107.0	24	134.0	33
27.0	17	52.0	4	83.0	27	108.0	33	135.0	33
28.0	14	53.0	5	84 .0	12	109.0	43	136.0	39
29.0	53	58.0	3	85.0	33	110.0	24	137.0	27
30.0	58	0.09	6	86.0	35	111.0	18	138.0	15
31.0	51	62.0	ю	87.0	69	112.0	36	139.0	12
				And the second s				140.0	18
								141.0	32
								142.0	15
	***	0000	***************************************		CECT TEND	77 080	***************************************	144.0	3
21 AGE 1 . 1 . 1 . 1 . 1	166931	IT ING TOO STREETS RELAYALIEN	0			:		145.0	m
				- 1				147.0	9
This sample size summary is	ze summe	ary is applicable	to	figures 30 thru	33.			156.0	e 1
								158.0	5
								160.0	
							And the second of the second o	162.0	01
								163.0	2
	-	which is the second or and the second of the						164.0	0 4
								100.0	
							The second secon	168.0	m

Figure 30

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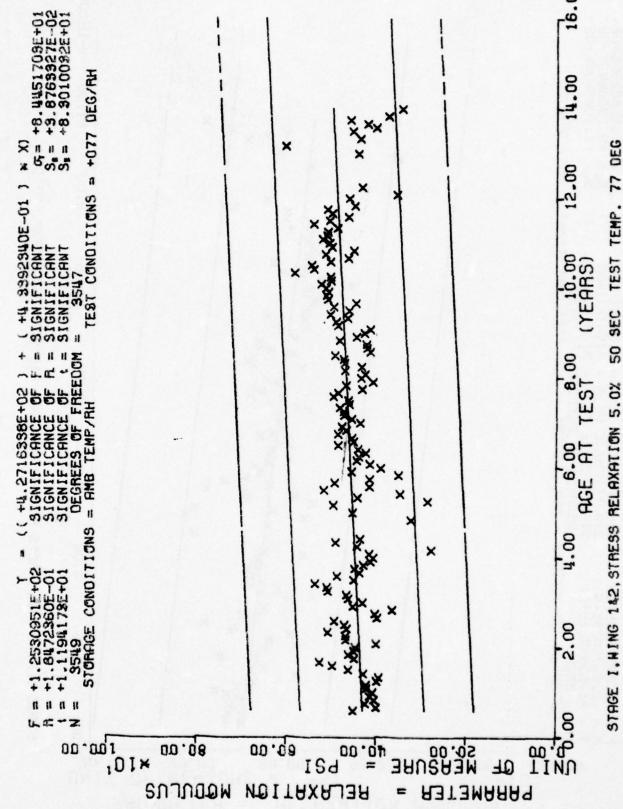
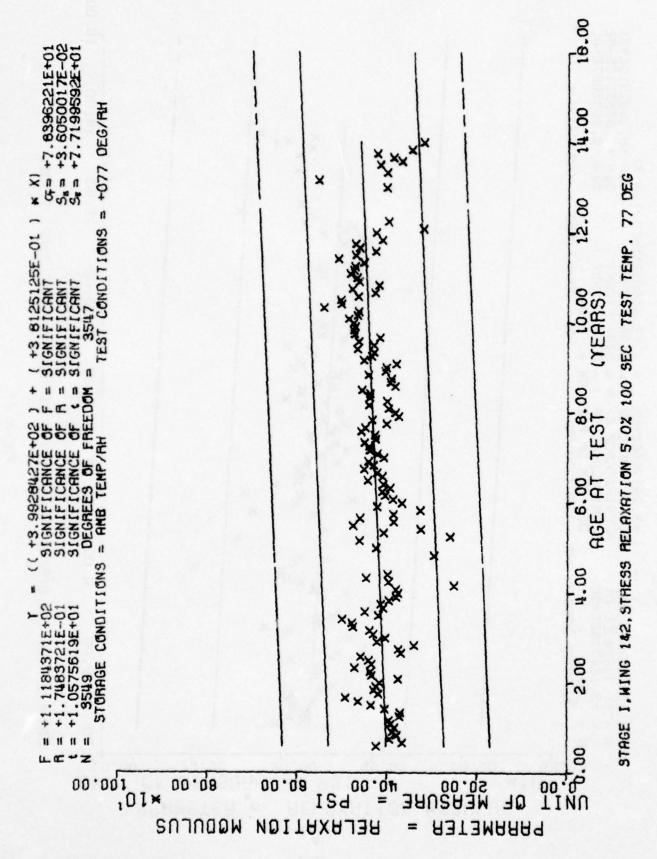
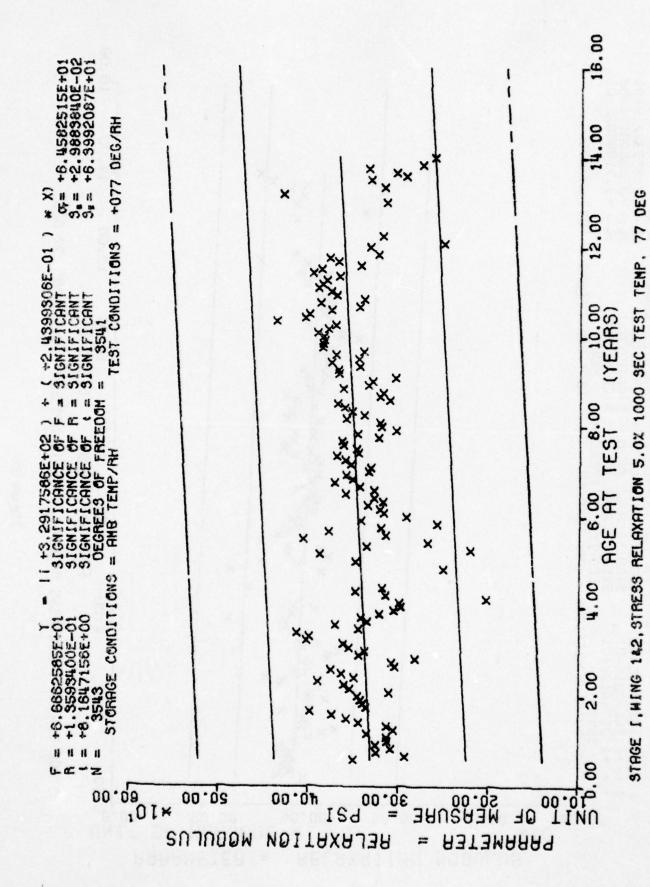


Figure 31





S) SAMPL 2 2 3 3 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	ES (MONTHS) 3 31.0 4 32.0 6 34.0 6 35.0	SAMPLES	(MINTHS)	SAMPLES	(MONTHS)	SAMPLES	(MUNTHS)	SAMPLES
0000000000	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8							
000000000		150	63.0	18	88.0	525	113.0	138
• • • • • • • • •		63	64.0	54	80.0	585	114.0	153
000000		06	. 0.59	£	0.06	610	115.0	87
		72	66.0	30	01.0	466	116.0	66
00000		74	67.3	¢	92.0	528	117.0	28
		66	68.0	21	03.0	302	118.0	143
000	37.3	19	0.69	35	94.0	346	119.9	121
000		77	70.0	22	95.0	161	120.0	120
	5 39.0	68	71.0	87	0.96	180	121.0	15
		49	72.0	7.8	97.0	180	122.0	72
15.0		66	73.0	63	0.86	183	123.0	42
17.0	42.0	96	74.3	144	0.06	161	124.0	27
	7 43.0	174	75.0	102	0.001	198	125.0	45
	2 44.0	223	76.0	105	101.0	159	126.0	33
0	7 45.0	234	77.0	114	102.0	171	127.0	33
		212	78.0	120	103.0	171	128.0	21
	3 47.0	234	79.0	117	104.0	195	129.0	2.3
		176	80.0	150	105.0	195	130.0	C. N.
24.0 37	7 49.0	138	81.0	168	106.0	213	131.0	. 54
25.0 141		87	82.0	207	107.0	117	132.0	15
26.0 218		57	83.0	1.00	108.0	207	133.0	6
	52.0	25	84.0	308	109.0	126	1 24.0	15
28.0	7 53.0	56	85.0	180	110.0	156	1.3.0	45
29.0 243	3 57.0	£	86.0	195	1111.0	195	1 30.0	51
30.0	60.09	3	87.0	552	112.0	171	137.3	15
							138.0	27

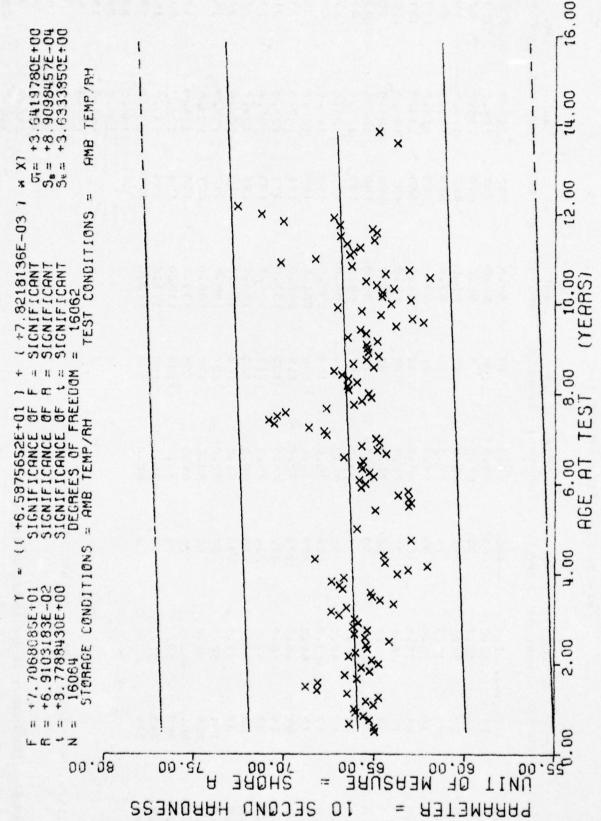
WING 182, HARDNESS SHOPE A, 10 SECOND PROPELLANT

~ G & G & W W W &

140.0 1441.0 1441.0 1444.0 1640.0 1660.0

This sample size summary is applicable to figure 34.

*



WING 142, HARDNESS SHORE A, 10 SECOND PROPELLANT

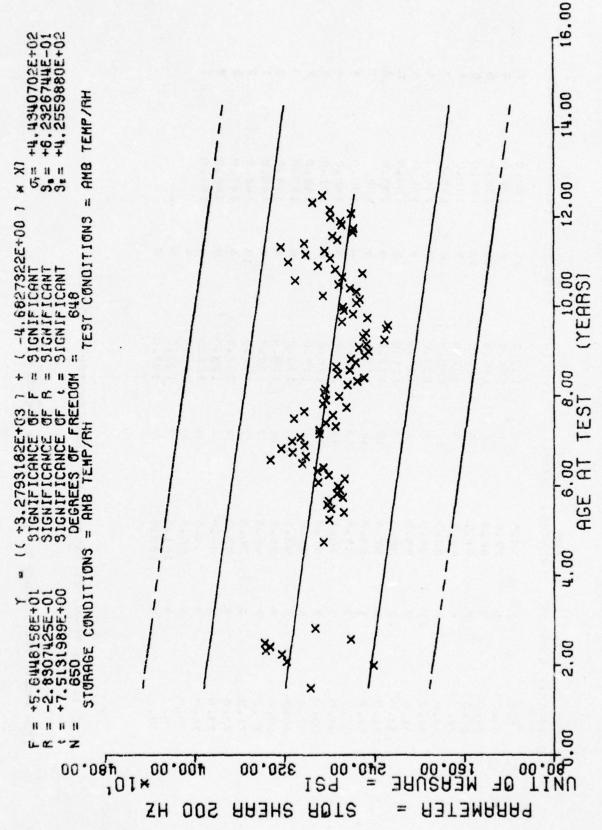
34

Figure

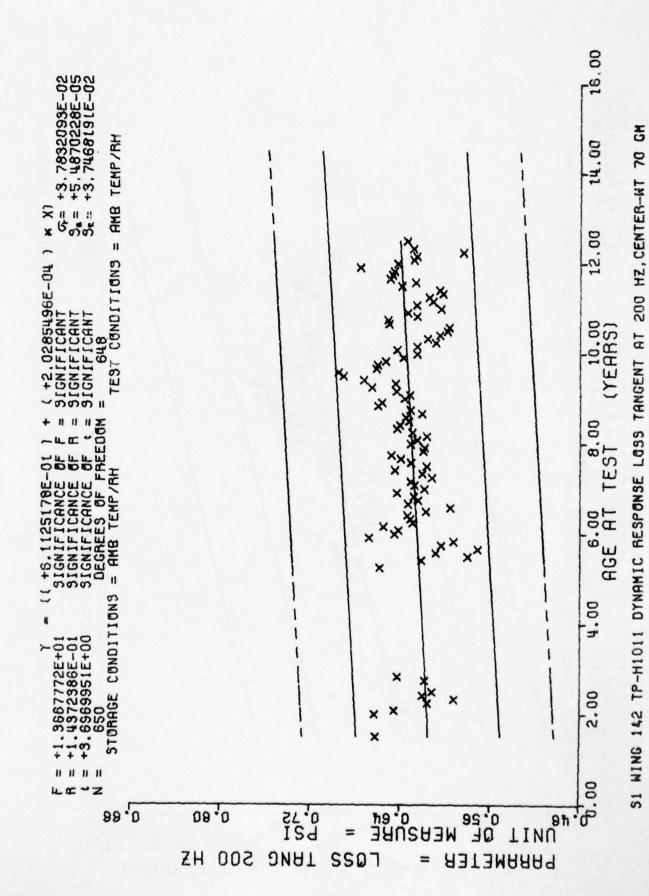
	SAMPLES	-	4	9	2	4	2	4	S	9	8		4	4	•	2	3	2	1	2	2	2				
AGE	(MONTHS)	128.0	129.0	130.0	131.0	132.0	133.0	134.0	135.0	136.0	137.0	138.0	139.0	140.0	141.0	142.0	143.0	144.0	145.0	146.0	147.0	148.0	150.0			
a z	SAMPLES	=	9	9	13	n	9	7	7	9	4	3	9	3	9	80	8	4		10	9	2	4	4	ır.	n
AGE	(MONTHS)	103.0	104.0	105.0	106.0	107.0	108.0	109.0	110.0	1111.0	112.0	113.0	114.0	115.0	116.0	117.0	118.0	119.0	120.0	121.0	122.0	123.0	124.0	125.0	126.0	127.0
ď	SANOLES	ß	S	S	0	6	11	83	٩	6	14	14	13	45	33	28	23	10.	7	7	6	•	4	0	7	7
AGE	(SHINGW)	78.0	79.0	80.0	81.0	82.0	83.0	84.0	85.0	6.98	87.0	88.0	89.0	0.06	91.0	95.0	93.0	0.46	95.0	36.0	97.0	98.0	0.66	100.0	101.0	102.0
CZ	SAMPLES		•		7	α	æ	1.1	3	2	2	1	3	3	2	4	3	4	1	3	1	1		7	6	0
AGE	(SHINLA)	18.0	24.0	25.0	27.0	28.0	29.0	30.0	31.0	33.0	34.0	57.0	63.0	65.0	66.0	67.0	69.0	69.0	70.0	71.0	72.0	73.0	74.0	75.0	76.3	77.0

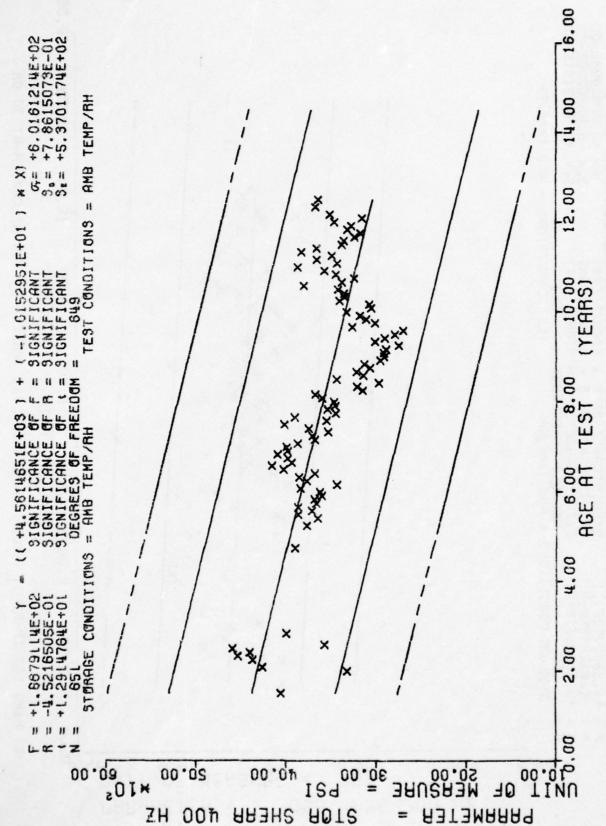
WING 182 SI TP-HIGH DYNAMIC RESEDNSE, CENTER-WT 70 GM.

This sample size summary is applicable for figures 35 thru 38.



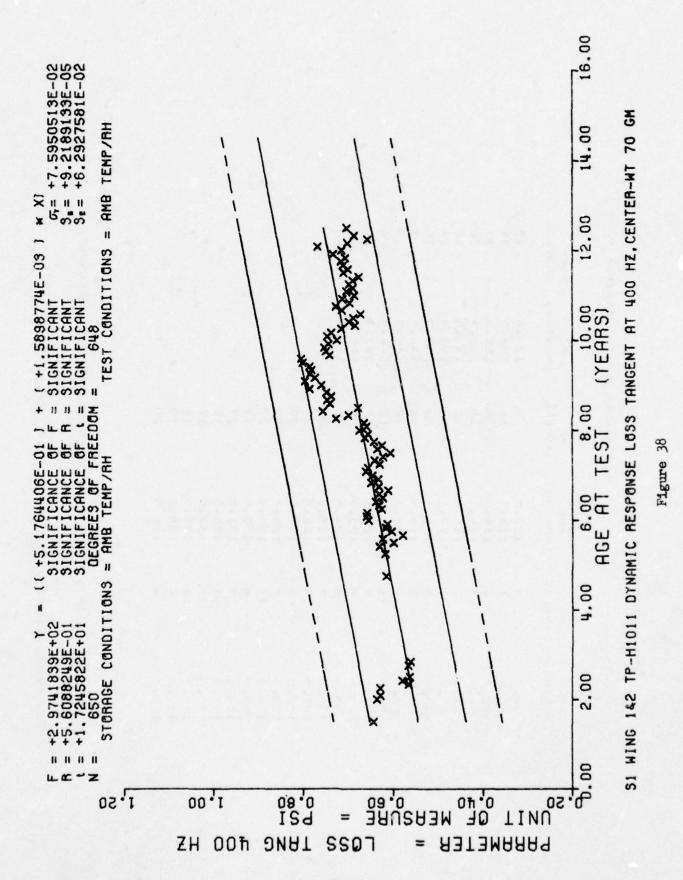
WING 142 ST TP-HIDLE DYNAMIC RESPONSE, CENTER-WT 70 GM, STOR SHEAR AT 200 HZ





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WING 142 SI TP-HIDLI DYNAMIC RESPONSE, CENTER-WT 70 GM, STOR SHEAR AT 400 HZ



- 57 -

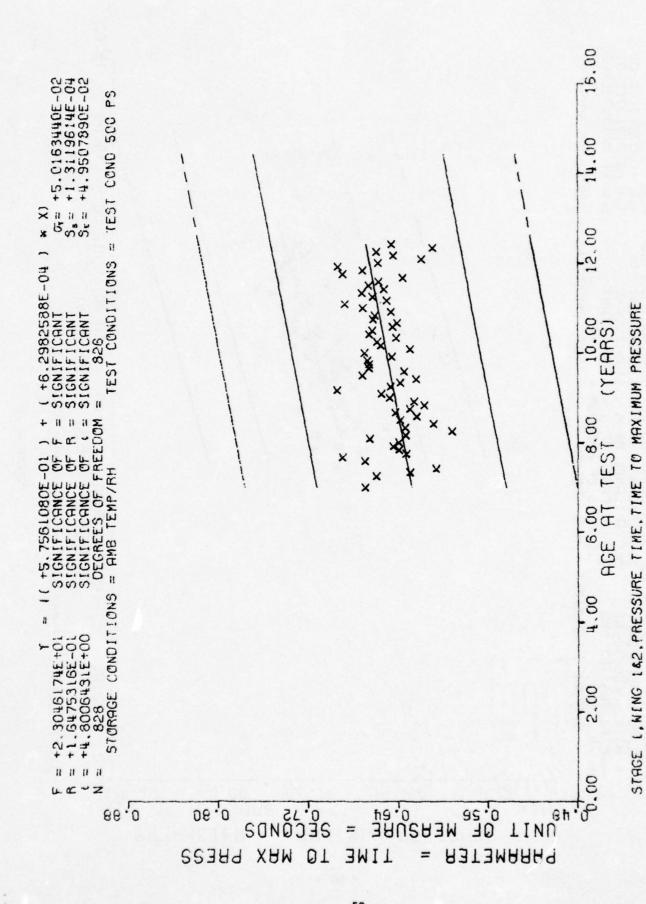
*** SAMPLE SIZE SUMMARY ***

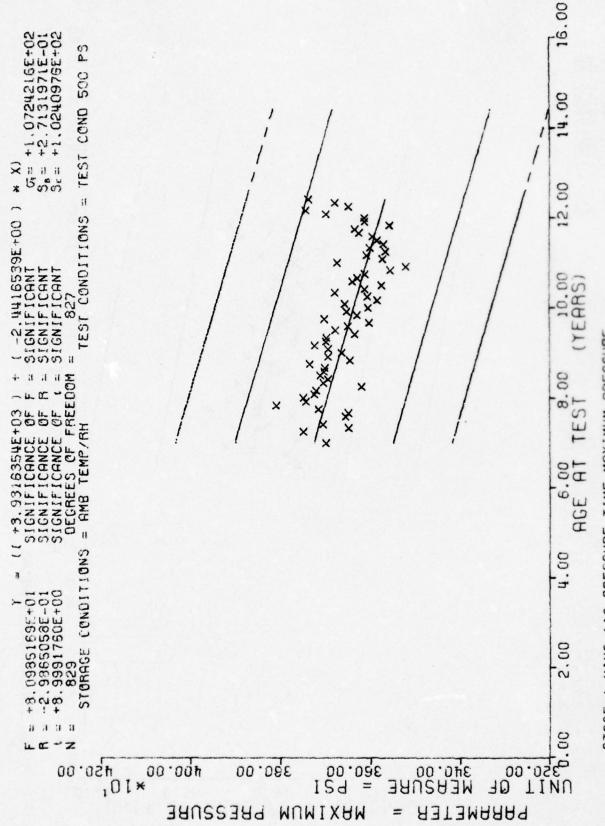
a،۷	SAMPLES	47	24	17	56	12	24	91	1	۴,	*	~	~	6												,
AGE	(MONTHS)	137.0		139.0		141.0	•	143.0	144.0	145.0	. 146.0		148.0	149.0												
2	SAMPLES	O.	11	4	25	15	17	23	18	19	15	10	36	15	30	24	39	30	27	- 21	27	15	10	14	19	50
AGE	(MONTHS)	115.0	113.0	114.0	115.6	116.0	117.3	118.3	119.0	120.0	121.0	122.3	123.0	124.0	125.0	126.0	127.0	128.0	129.0	130.0		132.0	133.0	134.0	135.0	136.0
NE	SAMPLES	2	-	2	۴,	۳.	-	r)	~	~		r	u.	60	7	10	a	ľ	10	9	7	11	¥1	16	4	4-
A 55	(SH INCW)	64.0	87.0	88.0	0.00	01.0	0.30	43.0	0.06	0.35	05.6	6.79	03.6	- 00°00	100.0	101.0	-102.0	163.0	104.0	165.6	106.0	107.0	109.0	100.0	110.0	111.0

STAGE 1.WING 182, PRESSURE TIME, TIME TO MAXIMUM PRESSURE

6.700 a Ve

This sample size summary is applicable to figures 39 and 40.





STAGE 1, WING 142, PRESSURE TIME, MAXIMUM PRESSURE

Pigure 40

*** SAMPLE SIZE SUMMARY ***

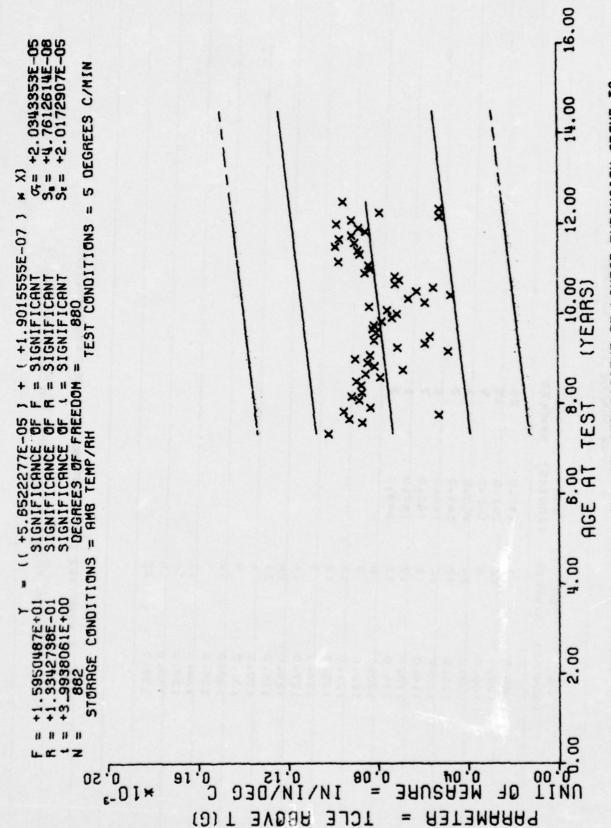
	(MONTHS)	SAMPLES	(MONTHS)	SAMPLES	(MONTHS)	SAMPLES		
	88.0	in	117.0	19	143.0	33		
-	91.0	9	118.0	42	144.0	18		
	92.3	9	119.0	43	145.0	15		
-	93.0	6	150.0	62	146.0	5		
	94.1	0	121.0	50	147.0	9		
	95.3	5	122.0	15	148.0	6		
	6.26	10	123.0	13	150.0	m		
-	930	3	124.0	18				
	0.66	6	125.0	6				
1	10100	-6	126.0	- 12				
	102.0	.9	127.0	18				
-	193.9	12	128.0	- 54				
	104.0	6	129.0	30				
-	105.0	-	130.0	30				
	106.0	6	131.0	24				
-	107.0	24	132.0					
	108.0	12	133.0	12				
	169.0	- 54	134.0	15				
	110.0	9	136.0	18				
1	1110	-6	137.0	15			-	
	112.0	9	138.0	30				
-	11300	\$3	139.0					-
	114.0	6	140.0	6				
-	11500		141.0					
	116.0	18	142.0	54				

TP-H1011 THERMAL COEFFICIENT OF LINEAR EXPANSION W1116 162 STAGE 1

This sample size summary is applicable for figures 41 and 42.

Figure 41

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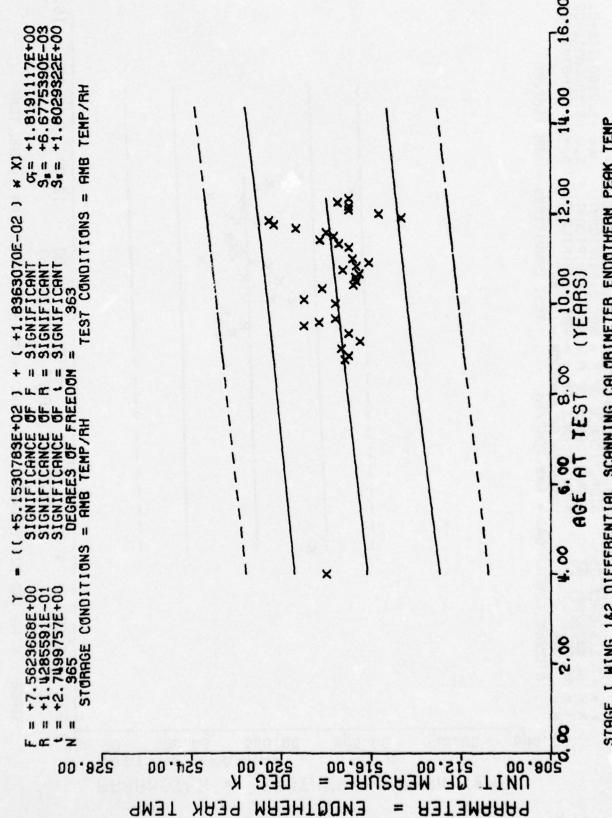
WING 142 STAGE 1 TP-H1011, THERMAL COEFFICIENT OF LINEAR EXPANSION ABOVE TG Figure 42

*** SAMPLE SIZE SUMMARY ***

SAMPLES	23		•	•	m	\$	7	9	m								•								
(MONTHS)	140.0	141.0	145.0	143.0	144.0	145.0	146.0	147.0	148.0																
SAMPLES	8	12	9	42	12	21	9	12	15	6	6	16	15	3	21	61		6	0	12	1		14	9	22
(MONT HS)	48.0	105.0	106.0	108.0	110.0	112.0	114.0	115.0	116.0	120.0	121.0	124.0	125.0	126.0	127.0	128.0	129.0	130.0	131.0	132.0	135.0	136.0	137.0	138.0	139.0

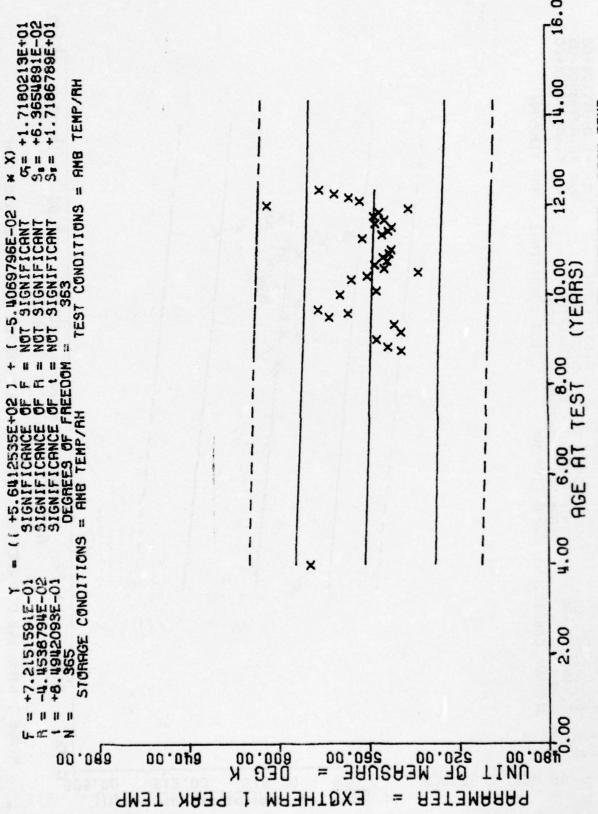
STAGE I WING 162 DIFFERENTIAL SCANNING CALORIMETER

This sample size summary is applicable for figures 43 thru 45.



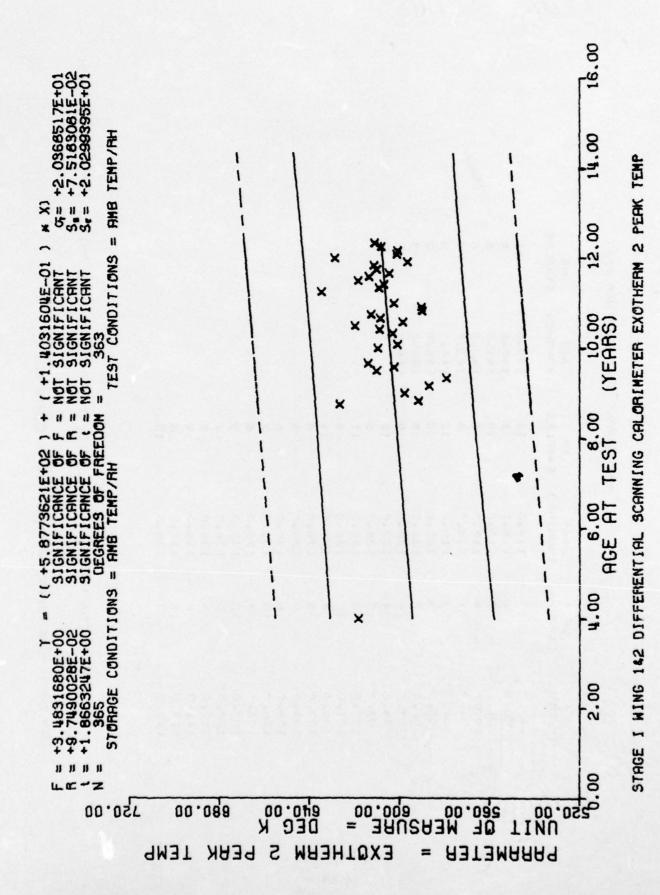
STAGE I WING 142 DIFFERENTIAL SCANNING CALORINETER ENDOTHERN PEAK TEMP

Figure 43



STAGE I WING 142 DIFFERENTIAL SCANNING CALORIMETER EXOTHERM I PERK TEMP

Figure 44



*** SAMPLE SIZE SUMMARY ***

			0 1 10000		
MONTHS)	SAMPLES	(WONTHS)	SAMPLES	(MONTHS)	SAMPLES
12.6	10	114.0	12	139.0	=
88.0	-	115.0	v	140.0	4
01.0	2	116.0	10	141.0	S
05.0	9	117.0	9	142.0	2
03.0	-	118.0	ø	143.0	7
0.40	M)	110.0	12	144.0	S
95.0	8	120.0	œ	145.0	2
0.96	m	121.0	α.	146.0	m
97.0	4	122.0	٥	148.0	8
98.6	4	123.0	12		
0.00	10	124.0	S		
100.0	7	125.0			
161.0	1.0	126.0	6		
102.0	æ	127.0	11	A. S.	
103.0	o	128.0	80		
104.0	0	150.0	4		
105.0	٠	130.0	9		
106.0	10	131.6	7		
107.0	· · · · · · · · · · · · · · · · · · ·	132.0		And the second s	
108.0	12	133.0	6		
109.0	•	134.0	11		
110.0	œ	135.0	S 2		
1111.0	Œ	136.0	4		
112.0	12	137.0	9		
0 211	7	138.0	. 7		

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STAGE 1 WING 182 TP-H1011 IGNITABILITY, IGN THPESHOLD POINT, 168 CAL/SO CM/SEC

This sample size summary is applicable to figure 46

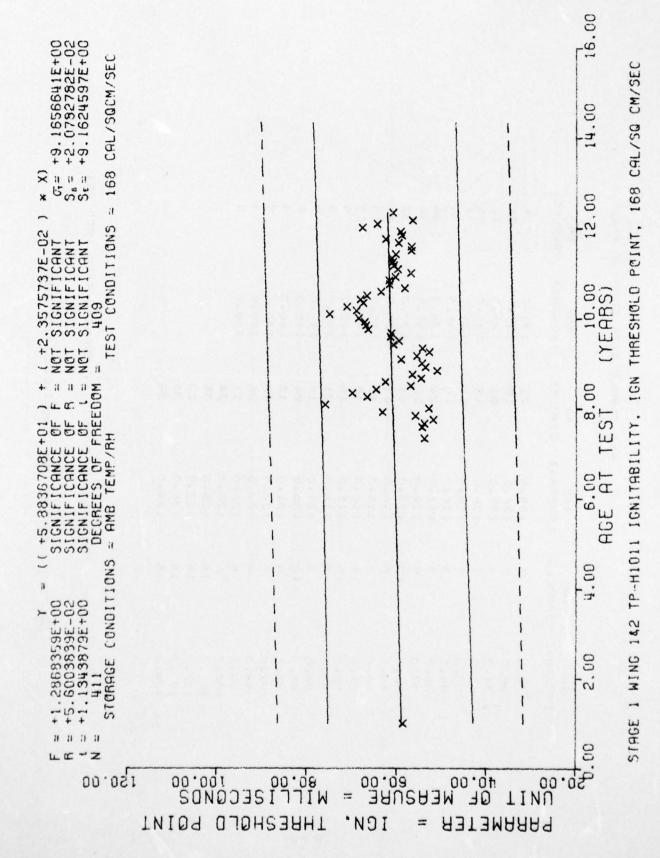
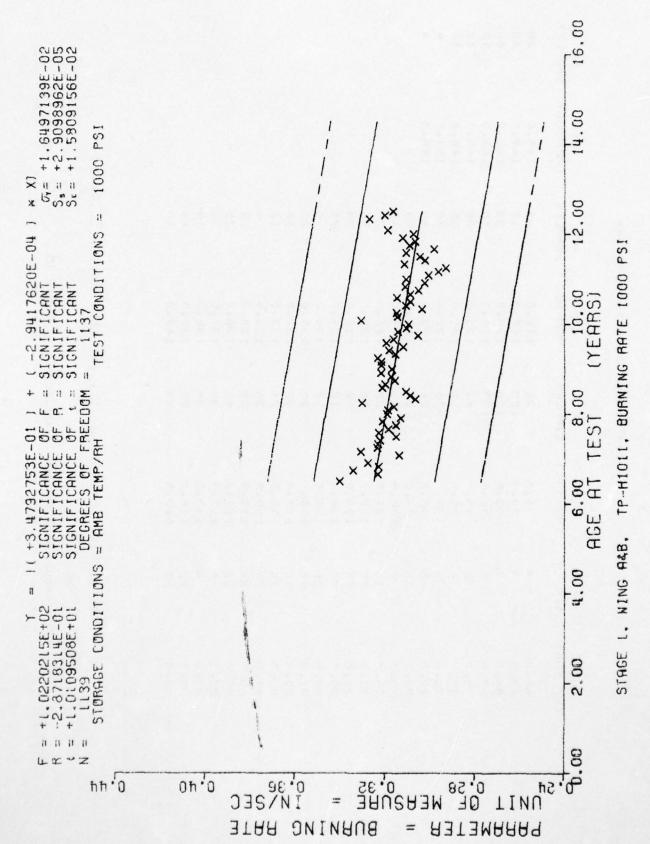


Figure 146

	SAMPLES	(MONTHS) S	SAMPLES	(MONTHS)	SAMPLES	
1	70	105.0	21	130.0	24	1
	æ	106.0	18	131.0	21	
	r	107.0	21	132.0	12	
	14)	108.0	-18	133.0.	56	-
	6	100.0	15	134.0	27	
	٣	116.0	0	135.0	c	
	3	1111.0	24	136.0	36	
	0	112.0	27	137.0	30	
	12	113.0	21	138.0	33	
	9	114.0	21	139.0	48	-
	r.	115.0	18	140.0	18	
	14	116.0	18	141.0	18	
	15	117.0	45	142.0	6	
	m	118.0	21	143.0	c	
	8	119.0	18	144.0	0	
Party of the Party	15	120.0	24	145.0	9	
	6	121.0	18	146.0	3	
	8	122.0	18	148.0	6	
	0	123.0	- 56	149.0	3	-
	9	124.0	21	150.0	3	
	9	125.0	24			
	15	126.0	35	the second was been been seen to be	A COLUMN TO SERVICE STATE	
	18	127.0	23			
	18	128.0	36			
	-16	129.0	- 53			

STAGE 1, WING AEB, TP-HIDII. BUPNING RATE 1000 PSI

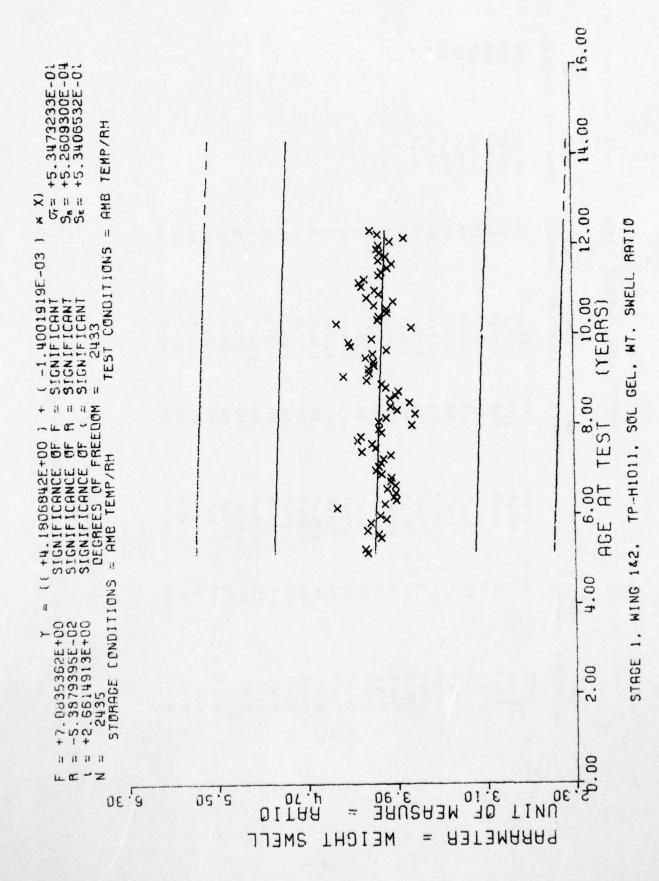
This sample size summary is applicable to figure 47.



HS) SAMPLES (MONTHS) SA	Mark land to the contract of the land of t	AGE	GN.	AGE	ű.	AGE	a v	AGE	22	
62.0 4 91.0 72 116.0 65.0 65.0 4 92.0 103 117.0 65.0 65.0 4 92.0 103 117.0 65.0 57.0 103 117.0 117.0 65.0 57.0 103 117.0 119.0 57.0 120.0 119.0 57.0 120.0 119.0 57.0 120.0 12		(MCNTHS)	· 12	(MONTHS)	SAMPLES	(MONTHS)	SAMPLES	(MONTHS)	SAMPLES	
65.0		62.0	4		72	116.0	48	141.0	28	
66.0 67.0 4 93.0 108 118.0 119.0 58.0 119.		63.0	æ	92.0	103	117.0	12	142.0	52	
67.0		0.99	4	93.0	108	118.0	32	143.0	40	
58.0 12 95.0 84 123.0 70.0 4 97.0 19 122.0 72.0 3 98.0 24 122.0 75.0 36 90.0 12 122.0 75.0 36 190.0 16 122.0 75.0 36 190.0 32 125.0 75.0 36 103.0 8 125.0 75.0 36 104.0 32 127.0 75.0 36 105.0 8 128.0 80.0 36 105.0 24 133.0 81.0 24 107.0 32 134.0 85.0 36 107.0 36 135.0 85.0 37 110.0 32 134.0 85.0 32 111.0 32 135.0 85.0 32 111.0 32 135.0 85.0 32 111.0 32 137.0 85.0 32 111.0 35 137.0 85.0 4 <		67.0	ď	0.40	130	119.0	16	144.0	12	
70.0 4 97.0 19 121.0 72.0 3 98.0 24 122.0 74.0 36 90.0 12 122.0 75.0 16 191.0 32 124.0 77.0 20 192.0 16 127.0 79.0 36 103.0 6 128.0 82.0 36 105.0 12 139.0 82.0 24 108.0 24 135.0 83.0 24 110.0 32 135.0 85.0 24 110.0 32 135.0 85.0 24 113.0 35 135.0 83.0 68 113.0 35 138.0		58.0	12	0.56	84	120.0	28	145.0	12	
71.0 4 97.0 19 122.0 72.0 36 98.0 24 123.0 74.0 36 99.0 12 12 124.0 75.0 16 191.0 32 126.0 75.0 16 191.0 32 126.0 75.0 16 191.0 32 126.0 75.0 20 193.0 89.0 36 195.0 83.0 85.0 24 113.0 28 135.0 85.0 24 113.0 35 138.0 85.0 50.0 58 140.0 58 140.0 59.0 72 114.0 40 136.0 58 137.0 58 114.0 59.0 72 114.0 72 113.0 72 113.0 72 113.0 72 113.0 72 113.0 72 113.0 72 113.0 72 113.0 72 113.0 72 114.0 72 113.0 72 114.0 72 113.0 72 114.0 72 114.0 72 114.0 72 114.0 72 113.0 72 114.0 7		70.07	7	0.96	50	121.0	20	146.0	12	
72.0 36 99.0 12 124.0 75.0 75.0 16 190.0 16 127.0 75.0 16 191.0 32 126.0 77.0 20 104.0 16 127.0 75.0 89.0 36 193.0 82.0 82.0 86.0 24 109.0 28 135.0 85.0 85.0 85.0 68 133.0 68		71.0	4	97.0	61	122.0	99	147.0	4	
75.0 36 90.0 12 124.0 75.0 16 190.0 16 125.0 77.0 20 193.0 16 127.0 79.0 36 193.0 8 128.0 82.0 40 197.0 32 133.0 85.0 24 190.0 28 135.0 85.0 24 110.0 28 135.0 85.0 24 113.0 32 137.0 85.0 24 113.0 32 137.0 85.0 25 111.0 40 136.0 86.0 32 111.0 40 136.0		72.0	3	98.0	24	123.0	40	148.0	4	
75.0		74.0	36	0.06	. 12	124.0	28			
75.0 16 191.0 32 126.0 2 77.0 20 192.0 16 127.0 4 78.0 36 193.0 8 128.0 2 81.0 24 195.0 32 132.0 8 85.0 24 110.0 28 133.0 8 85.0 32 111.0 40 136.0 3 85.0 32 111.0 40 136.0 3 83.0 72 114.0 40 130.0 2 83.0 72 114.0 70.0 68 130.0 2		75.0	B	196.0	91	125.0	48	And the second of the second		
73.0 20 102.0 16 127.0 2 79.0 36 103.0 8 128.0 2 80.0 36 105.0 12 129.0 2 80.0 36 105.0 32 131.0 2 83.0 24 109.0 28 133.0 134.0 85.0 24 113.0 28 135.0 33 134.0 28 135.0 33 137.0 28 133.0 135.0 33 137.0 28 133.0 68 113.0 28 135.0 28 130.0 28 130.0 28 130.0 28 130.0 28 140.0		75.0	16	101.0	32	126.0	27			
79.0 36 193.0 8 128.0 2 89.0 79.0 36 105.0 12 129.0 2 89.0 36 105.0 12 130.0 2 131.0 2 82.0 24 133.0 132.0 85.0 24 135.0 28 135.0 33 85.0 32 137.0 32 137.0 33 138.0 68 113.0 68 114.0 40 130.0 28 140.0 440 130.0 28 140.0		77.0		102.0	16	127.0	44			
89.0 36 105.0 12 129.0 2 130.0 82.0 36 105.0 12 130.0 82.0 20 131.0 2 131.0 2 131.0 2 132.0 133.0 133.0 24 133.0 24 135.0 28 135.0 86.0 32 111.0 40 136.0 33 137.0 33 137.0 33 137.0 2 137.0 2 137.0 2 130.0 68 115.0 68 140.0 68 140.0		78.0	36	103.0	30	128.0	24			
89.0 36 105.0 12 130.0 8 105.0 12 130.0 8 131.0 8 132.0 132.0 132.0 132.0 133.0 133.0 134.0 85.0 24 133.0 135.0 86.0 32 1311.0 40 135.0 33 137.0 83.0 4 113.0 35 137.0 83.0 68 113.0 68 114.0 68 140.0 68 140.0	-	19.0	56	104.0	12	129.0	21			
82.0 40 107.0 32 132.0 83.0 24 109.0 24 133.0 24 133.0 85.0 24 110.0 28 135.0 85.0 24 113.0 40 135.0 87.0 20 1112.0 32 137.0 33.0 117.0 32 137.0 33.0 40 130.0 68 115.0 28 140.0	72	80.0	36	105.0	12	130.0	œ			
24 108.0 24 133.0 24 133.0 24 133.0 24 133.0 24 133.0 24 135.0 26 135.0 26 135.0 26 135.0 26 135.0 26 135.0 26 135.0 26 135.0 26 140.0 26 140.0			54	1.961	- 50	131.0	50		有 三 子 十二十二十二十二十二十二十二十二十二十二十二十二十二十二十二十二十二十二十	
24 108.0 24 133.0 24 109.0 36 134.0 32 111.0 40 136.0 4 113.0 35 138.0 72 114.0 40 130.0 68 115.0 28 140.0		82.0	40	107.0	32	132.0	91			
24 109.0 36 134.0 28 135.0 2 111.0 40 136.0 32 117.0 32 137.0 40 137.0 40 138.0 72 114.0 40 130.0 68 115.0 28 140.0		83.0	24	108.0	24	133.0	12			
24 110.0 28 135.0 32 111.0 40 136.0 20 112.0 32 137.0 4 113.0 35 138.0 72 114.0 40 130.0 68 115.0 28 140.0		84.0	24	109.0	36	134.0	4		The second secon	
32 111.0 40 136.0 20 112.0 32 137.0 4 113.0 35 138.0 72 114.0 40 130.0 68 115.0 28 140.0		85.0	24	110.0	28	135.0	œ			
20 112.0 32 137.0 4 113.0 35 138.0 72 114.0 40 130.0 68 115.0 28 140.0		86.0	32	111.0	40	136.0	35			
72 114.0 40 130.0 68 115.0 28 140.0		6.73	50		32	.137.0	35			
72 114.0 40 130.0		83.0	4	1,13.0	35	138.0	19			
115.0		87.0	72		40	130.0	28			
		6.06	- 69	115.6	28	140.0	40		1	

STAGE 1, WING 182, TP-HIGHT, SOL GEL, WT. SWELL PATIO

This sample size summary is applicable to figure 48.



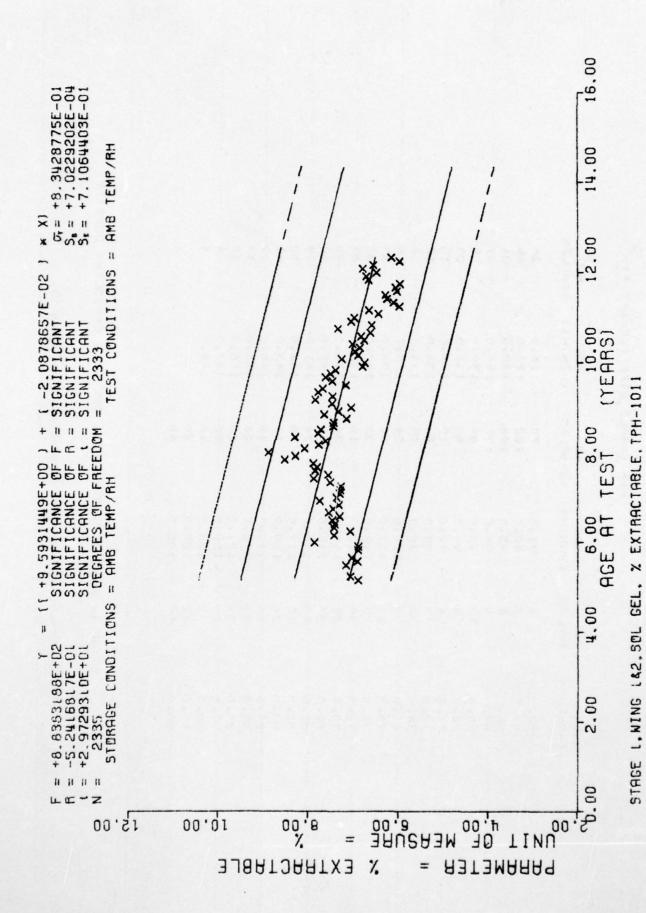
*** SAMPLE SIZE SUMMARY ***

SAVIDLES (MONTHS) SAMPLES (MONTHS) SAMPLES (MONTHS)		- 46F	N.	AGE	œ.	AGE	X X	AGE	9	
0		(MONTHS)		(SHINDM)	SAMPLES	(MONTHS)	SAMPLES	(MONTHS)	SAMPLES	
0 0		62.0	7	91.0	72		40	141.0	28	1
0 4 93.0 108 118.0 32 143.0 0 4 94.0 130 119.0 16 144.0 0 12 95.0 120.0 28 145.0 0 4 97.0 19 121.0 20 146.0 0 3 98.0 24 122.0 40 148.0 0 3 99.0 12 124.0 28 147.0 0 36 101.0 16 125.0 40 148.0 0 36 102.0 12 125.0 44 44 0 20 16 125.0 44 44 147.0 0 36 103.0 16 125.0 44 44 147.0 0 36 104.0 16 125.0 44 44 148.0 44 44 148.0 44 44 148.0 44 44 148.0 44		63.0	α.	92.0	103	117.0	12	142.0	52	
0 44.0 130 119.0 16 144.0 0 4 96.0 59 121.0 28 145.0 0 4 96.0 19.0 20 146.0 0 3 98.0 24 122.0 56 147.0 0 3 99.0 12 122.0 40 148.0 0 36 199.0 12 124.0 28 147.0 0 36 199.0 12 126.0 27 148.0 0 36 103.0 16 127.0 44 44 44 0 20 104.0 16 127.0 44		66.1	4	93.0	108	118.0	32	143.0	39	
0 4 96.0 84 120.0 26 145.0 0 4 97.0 19 121.0 20 146.0 0 3 98.0 24 122.0 56 147.0 0 3 98.0 12 122.0 56 147.0 0 36 199.0 12 124.0 28 147.0 0 36 190.0 12 125.0 44 44 0 36 103.0 12 125.0 24 44 0 36 104.0 12 129.0 21 24 0 36 105.0 12 130.0 24 16 140.0 20 0 24 105.0 24 135.0 4 4 112.0 4 4 0 24 109.0 24 135.0 4 4 113.0 24 135.0 4 4 113.0 4 <td></td> <td>67.0</td> <td>α</td> <td>0.46</td> <td>130</td> <td>119.0</td> <td>16</td> <td>144.0</td> <td>12</td> <td>-</td>		67.0	α	0.46	130	119.0	16	144.0	12	-
0 4 96.0 59 121.0 20 146.0 0 3 98.0 24 122.0 56 147.0 0 36 99.0 12 124.0 28 0 36 99.0 16 125.0 40 148.0 0 36 190.0 16 125.0 48 148.0 27 0 36 101.0 32 125.0 44 44 44 0 36 103.0 16 127.0 44 44 0 36 104.0 12 120.0 24 140.0 24 0 40 105.0 24 135.0 12 4 4 0 24 100.0 16 135.0 4 4 0 24 100.0 16 135.0 4 4 0 24 110.0 24 136.0 35 0		68.0	12	0.50	84	120.0	28	145.0	12	
0 4 97.0 19 122.0 56 147 0 36 98.0 24 123.0 40 148 0 36 99.0 12 124.0 28 0 8 199.0 16 125.0 48 0 20 102.0 16 125.0 44 0 36 103.0 16 127.0 44 0 36 104.0 12 129.0 21 0 36 104.0 12 129.0 21 0 36 105.0 12 130.0 8 0 40 107.0 20 131.0 9 0 24 109.0 32 134.0 4 0 24 109.0 32 135.0 19 0 24 110.0 24 136.0 35 0 24 113.0 20 137.0 20		72.0	4	0.96	69	121.0	20	146.0	12	
0 3 98.0 24 123.0 40 0 36 99.0 12 124.0 28 0 8 199.0 16 125.0 48 0 20 102.0 16 125.0 27 0 36 103.0 16 127.0 44 0 36 104.0 12 129.0 21 0 36 105.0 12 130.0 24 0 40 107.0 32 131.0 20 0 24 106.0 24 133.0 12 0 24 109.0 32 134.0 4 0 24 110.0 24 135.0 4 0 24 110.0 24 135.0 4 0 24 110.0 24 135.0 4 0 24 113.0 24 136.0 35 0	The second of th	74.0	4	97.0	51	122.0	99	147.0	4	
0 36 99.0 12 124.0 0 8 100.0 16 125.0 0 20 101.0 32 125.0 0 20 103.0 16 127.0 0 20 104.0 12 128.0 0 36 105.0 20 131.0 0 40 107.0 20 131.0 0 24 108.0 24 133.0 0 24 110.0 32 134.0 0 24 110.0 24 135.0 0 24 110.0 24 135.0 0 24 110.0 24 135.0 0 24 113.0 24 135.0 0 24 113.0 24 135.0 0 24 113.0 24 135.0 0 24 135.0 137.0 0 26 135.0 <td< td=""><td></td><td>72.0</td><td>m</td><td>98.0</td><td>24</td><td>123.0</td><td>40</td><td>148.0</td><td></td><td></td></td<>		72.0	m	98.0	24	123.0	40	148.0		
0 16 101.0 32 126.0 2 1 101.0 32 126.0 2 1 101.0 32 126.0 2 1 102.0 16 127.0 4 1 102.0 16 127.0 4 1 102.0 17.0 24 133.0 1 100.0 24 133.0 1 100.0 24 133.0 1 100.0 24 136.0 2 1 130.0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		74.0	36	0.66	12	124.0	28			
0 20 101.0 32 126.0 2 0 20 102.0 16 127.0 4 0 20 104.0 12 129.0 2 0 36 105.0 12 129.0 2 0 40 107.0 20 131.0 2 0 24 108.0 24 133.0 1 0 24 110.0 24 135.0 1 0 32 112.0 20 135.0 1 0 32 112.0 20 135.0 1 0 72 114.0 20 139.0 2		75.0		199.0	- 16	125.0	48	The same of the same of the same of		-
0 20 102.0 16 127.0 4 0 36 103.0 8 128.0 0 36 105.0 12 129.0 2 0 40 107.0 24 133.0 0 24 108.0 24 133.0 0 24 110.0 24 135.0 0 32 111.0 24 136.0 0 40 112.0 20 138.0		76.0	16	101.0	32	126.0	27			
0 20 104.0 12 129.0 2 20 105.0 12 130.0 2 20 105.0 12 130.0 2 20 131.0 2 2 132.0 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		77.0	20	192.0	16	127.0	44			
0 36 105.0 12 129.0 2 0 36 105.0 12 130.0 0 40 107.0 32 132.0 1 0 24 108.0 24 133.0 0 24 110.0 24 136.0 0 32 111.0 24 136.0 0 40 112.0 20 139.0		78.0	- 36	103.0	8	128.0	. 24		The state of the same of the s	-
0 36 105.0 12 130.0		79.0	20	104.0	12	129.0	21			
0 40 107.0 32 132.0 100.0 24 108.0 24 133.0 109.0 24 133.0 109.0 24 133.0 109.0 32 134.0 109.0 32 136.0 32 136.0 32 136.0 32 136.0 139.0 20 139.0 20 139.0 20 139.0 20 139.0 20 139.0 20 139.0 20 139.0 20 139.0 20 139.0 20 139.0 20 140.0 20 20 140.0 20 20 140.0 20 20 20 20 20 20 20 20 20 20 20 20 20	74	80.0	36	105.0	12	130.0	6 0			
0 40 107.0 32 132.0 1 1		81.0	- 99	106.0	- 50	131.0	- 50			1
0 24 108.0 24 133.0 1 0 24 109.0 32 134.0 0 30 32.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		82.0	40	107.0	32	132.0	16			
0 24 110.0 16 135.0 0 32 111.0 24 136.0 0 4 112.0 20 137.0 0 72 114.0 20 139.0 0 68 115.0 16 140.0		83.0	24	1.08.0	54	133.0	12			
0 24 110.0 16 135.0 0 32 111.0 24 136.0 0 4 112.0 20 138.0 0 68 115.0 16 140.0		84.0	-24	10000	32	134.0	4			1
0 32 111.0 24 136.0 3 0 20 137.0 3 1 113.0 20 138.0 1 1 72 114.0 20 139.0 2 0 68 115.0 16 140.0		85.0	54	110.0	16	135.0	80			
7 2 114.0 20 139.0 72 138.0 0 68 115.0 16 140.0		86.0	32	111.0	24	136.0	35			
72 114.0 20 138.0 72 114.0 0 58 115.0 15.0 1.15.0		87.A	- 56	112.0	-50	137.0	32			and a
0 72 114.0 .20 139.0 0 68 115.0 .6 140.0		88.7	4	113.0	20	138.0	61			
0 68 115.0 16 140.0		89.0	72	114.0	.20	139.0	28			
		0.06	89	115.0	91	140.0				-

STAGE 1, WING 182, SOL GEL, % EXTRACTABLE, TPH-1011

N. C.

This sample stze summary is applicable to figure 49.



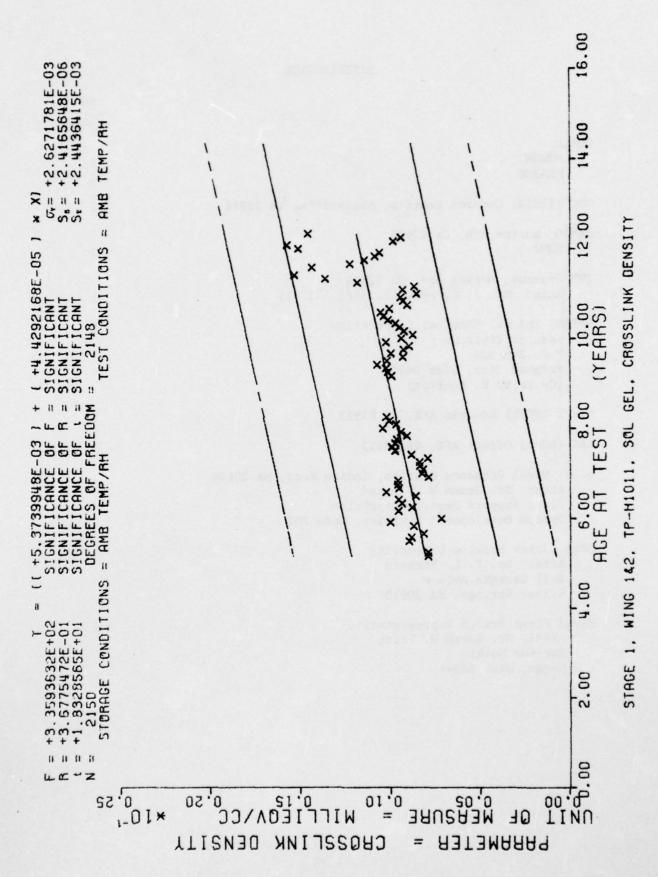
*** SAMPLE SIZE SUMMARY ***

(MONTHS)	SAMPLES	(MUNTHS)	SAMPLES	(MONTHS)	SAMPLES	
65.9	4	91.0	72	126.0	28	
63.0	60	. 92.0	103	127.0	45	
.0.99	4	93.0	108	128.0	24	
47.9	. 8	94.0	130	129.0	- 21	-
68.0	12	95.0	84	130.0	60	
70.0	4	0.96	65	131.0	20	
71.0	•	97.0	19	132.0	16	
72.0	3	0.86	24	133.0	12	
74.0	36	0.66	12	134.0	•	The state of the state of
75.0	6	1100	28	135.0	6	
76.0	16	111.0	40	136.0	35	
77.0	20	112.0	32	137.0	32	
78.0	36	113.9		138.0	- 50	
79.0	20	114.0	36	139.0	28	
60.09	36	115.0	16	140.0	40	
81.0	- 56	11600	54	141.0	- 28	- designation of the latest and the
82.0	40	117.0	æ	142.0	52	
83.0	24	118.0	16	143.0	40	
84.0	54		91	144.0	12	
85.0	24	120.0	. 28	145.0	12	
86.0	3.2	121.0	20	146.0	12	
87.0	- 62	122.0	- 56	147.0	4	
38.0	4	123.7	04	148.0	4	
0.68	72	124.0	28			

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STAGE 1. WING 182, TP-H1011, SOL GEL, CROSSLINK DENSITY

This sample size summary is applicable to figure 50.



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Continued from Block 20:

An analysis of all parameters indicates that no potential problems are expected in the propellant for at least two years past the oldest data point.

Data stored in the GO85 System were plotted utilizing the IBM 360-65 Computer and CAL-COMP Plotter. The data range at any age can be found by suitable inquiry of the GO 85 System.

Each point on the regression plot represents the mean of all samples at that particular age. The number of specimens at each point is indicated on the sample size summary sheet accompanying each regression plot or group of regression plots.